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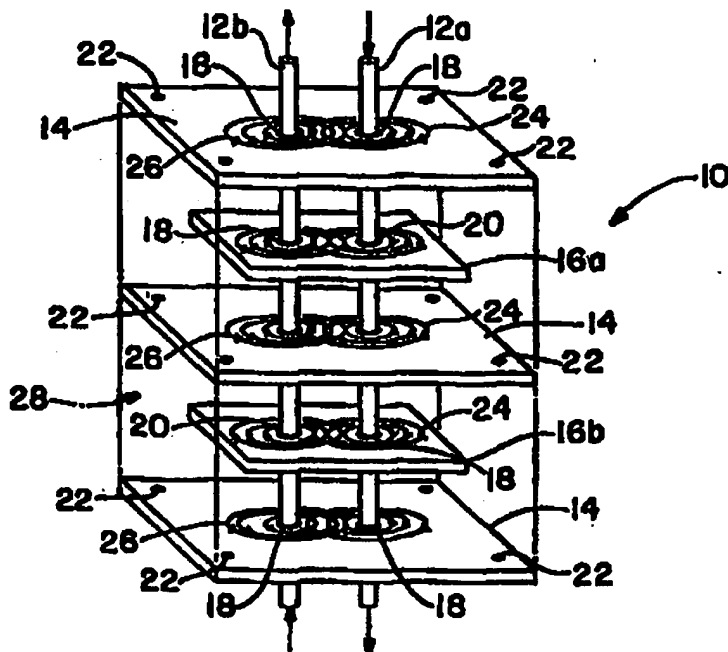
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(54) Title: PAIRED MULTI-LAYERED DIELECTRIC INDEPENDENT PASSIVE COMPONENT ARCHITECTURE RESULTING IN DIFFERENTIAL AND COMMON MODE FILTERING WITH SURGE PROTECTION IN ONE INTEGRATED PACKAGE

(57) Abstract

The present invention relates to a passive electronic component architecture (10) employed in conjunction with various dielectric (16) and combinations of dielectric materials to provide one or more differential and common mode filters (12) for the suppression of electromagnetic emissions and surge protection. The architecture allows single or multiple components (22) to be assembled within a single package (10) such as an integrated circuit or connector. The component's architecture is dielectric independent and provides for integration of various electrical characteristics within a single component to perform the functions of filtering, decoupling, fusing and surge suppression, alone or in combination.



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**PAIRED MULTI-LAYERED DIELECTRIC INDEPENDENT PASSIVE
COMPONENT ARCHITECTURE RESULTING IN DIFFERENTIAL AND
COMMON MODE FILTERING WITH SURGE PROTECTION IN ONE
INTEGRATED PACKAGE**

Technical Field

This application is a continuation-in-part of application Serial No. 09/056,379 filed April 7, 1998, which is a continuation-in-part of application Serial No. 09/008,769 filed January 19, 1998, which is a continuation-in-part of application Serial No. 08/841,940 filed April 8, 1997. The present invention relates to a filter for protecting electronic circuitry from
5 electromagnetic field interference (EMI), over voltages and preventing electromagnetic emissions. More specifically, this invention relates to a multi-functional electronic component whose physical architecture suppresses unwanted electromagnetic emissions, both those received from other sources and those created internally within electronic circuitry by differential and common mode currents. In addition, due to the electronic component's
10 physical architecture and material composition, over voltage surge protection and magnetic properties can be integrally incorporated with the differential and common mode filtering.

Background of the Invention

The majority of electronic equipment produced presently, and in particular computers, communication systems, automobiles, military surveillance equipment, stereo and home
15 entertainment equipment, televisions and other appliances include miniaturized components to perform new high speed functions and electrical interconnections which according to the materials from which they are made or their mere size are very susceptible to stray electrical energy created by electromagnetic interference or voltage transients occurring on electrical lines. Voltage transients can severely damage or destroy such micro-electronic components
20 or contacts thereby rendering the electronic equipment inoperative, and requiring extensive

repair and/or replacement at great cost.

Electrical interference in the form of EMI or RFI can be induced into electrical lines from such sources as radio broadcast antennas or other electromagnetic wave generators. EMI can also be generated from the electrical circuit which is desired to be shielded from

5 EMI. Differential and common mode currents are typically generated in cables and on circuit board tracks. In many cases fields radiate from these conductors which act as antennas. Controlling these conducted/radiated emissions is necessary to prevent interference with other circuitry or other parts of the circuit generating or sensitive to the unwanted noise. Other sources of interference are generated from equipment coupled to the electrical lines,

10 such as computers, switching power supplies and a variety of other systems, which may generate significant interference which is desired to be eliminated to meet international emission and/or susceptibility requirements.

Transient voltages occurring on electrical lines can be induced by lightning which produces extremely large potentials in a very short time. In a similar manner, nuclear

15 electromagnetic pulses (EMP) generate even larger voltage spikes with faster rise time pulses over a broad frequency range which are detrimental to most electronic devices. Other sources of large voltage transients are found to be associated with voltage surges occurring upon the switching off or on of some electronic power equipment as well as ground loop interference caused by varying ground potentials. Existing protection devices, primarily due to their

20 architecture and basic materials, do not provide adequate protection in a single integrated package.

Based upon the known phenomenon of electromagnetic emissions and transient voltage surges a variety of filter and surge suppression circuit configurations have been

designed as is evident from the prior art. A detailed description of the various inventions in the prior art is disclosed in U.S. Patent No. 5,142,430, herein incorporated by reference.

The '430 patent itself is directed to power line filter and surge protection circuit components and the circuits in which they are used to form a protective device for electrical equipment. The circuit components comprise wafers or disks of material having desired electrical properties such as varistor or capacitor characteristics. The disks are provided with electrode patterns and insulating bands on surfaces thereof which coact with apertures formed therein so as to electrically connect the components to electrical conductors of a system easily and effectively. These electrode patterns act in conjunction with one another to form common electrodes with the material interposed there between. The '430 patent was primarily directed toward filtering paired lines. The present invention improves on the paired line concept by refining and adapting the concept for use with low voltage low current data communication lines as well as arrangements directed towards high voltage industrial and home applications such as three phase power lines, electric motor noise filtering, LANs and other computer and electronic devices.

Therefore, in light of the foregoing deficiencies in the prior art, the applicant's invention is herein presented.

Summary of the Invention

Based upon the foregoing, there has been found a need to provide a multi-functioning electronic component which attenuates electromagnetic emissions resulting from differential and common mode currents flowing within electronic circuits, single lines, pairs of lines and multiple twisted pairs. Because of the sensitive nature of electronic technology there is also a need for combining electromagnetic filtering with surge protection to eliminate the

susceptibility to over voltages and emissions from external sources. Due to the highly competitive nature of today's electronic industry such a differential and common mode filter/surge protector must be inexpensive, miniaturized, low in cost and highly integrated to be incorporated into a plurality of electronic products.

5 It is therefore a main object of the invention to provide an easily manufactured and adaptable multi-functional electronic component which filters electromagnetic emissions caused by differential and common mode currents.

 It is another object of the invention to provide a protective circuit arrangement which may be mass produced and adaptable to include one or more protective circuits in one
10 component package to provide protection against voltage transients, over voltages and electromagnetic interference.

 Another object of the invention is to provide protective circuits having an inherent ground which provides a path for attenuating EMI and over voltages without having to couple the hybrid electronic component to circuit or earth ground.

15 These and other objects and advantages of the invention are accomplished through the use of a plurality of common ground conductive plates surrounding corresponding electrode plates separated by a material which exhibits any one or a combination of a number of predetermined electrical properties. By coupling pairs of conductors to the plurality of common ground conductive plates and selectively coupling the conductors to electrode
20 plates, line-to-line and line-to-ground component coupling is accomplished providing differential and common mode electromagnetic interference filtering and/or surge protection. The circuit arrangement comprises at least one line conditioning circuit component constructed as a plate. Electrode patterns are provided on one surface of the plate and the

electrode surfaces are then electrically coupled to electrical conductors of the circuit. The electrode patterns, dielectric material employed and common ground conductive plates produce commonality between electrodes for the electrical conductors which produces a balanced (equal but opposite) circuit arrangement with an electrical component coupled line-to-line between the electrical conductors and line-to-ground from the individual electrical conductors.

The particular electrical effects of the differential and common mode filter are determined by the choice of material between the electrode plates and the use of ground shields which effectively house the electrode plates within one or more Faraday cages. If one specific dielectric material is chosen the resulting filter will be primarily a capacitive arrangement. The dielectric material in conjunction with the electrode plates and common ground conductive plates will combine to create a line-to-line capacitor and a line-to-ground capacitor from each individual electrical conductor. If a metal oxide varistor (MOV) material is used then the filter will be a capacitive filter with over current and surge protection characteristics provided by the MOV-type material. The common ground conductive plates and electrode plates will once again form line-to-line and line-to-ground capacitive plates providing differential and common mode filtering except in the case of high transient voltage conditions. During these conditions the MOV-type varistor material, which is essentially a non-linear resistor used to suppress high voltage transients, will take effect to limit the voltage which may appear between the electrical conductors.

In a further embodiment a ferrite material may be used adding additional inherent inductance to the differential and common mode filter arrangement. As before, the common ground conductive and electrode plates form line-to-line and line-to-ground capacitive plates

with the ferrite material adding inductance to the arrangement. Use of the ferrite material also provides transient voltage protection in that it will become conductive at a certain voltage threshold allowing the excess transient voltage to be shunted to the common ground conductive plates, effectively limiting the voltage across the electrical conductors.

5 Numerous other arrangements and configurations are also disclosed which implement and build on the above objects and advantages of the invention to demonstrate the versatility and wide spread application of differential and common mode filters within the scope of the present invention.

Brief Description of the Drawings

10 FIG. 1 shows an exploded perspective view of a differential and common mode filter in accordance with the present invention;

FIG. 1A shows an exploded perspective view of an alternate embodiment of the filter shown in FIG. 1;

FIG. 2 provides schematic diagrams of the filter shown in FIG. 1 with FIG. 2a
15 being a pure schematic representation and FIG. 2b being a schematic representation of the physical architecture;

FIG. 3 is a logarithmic graph comparing the filter of FIG. 1 with a filter comprised of prior art chip capacitors showing insertion loss as a function of signal frequency;

FIG. 4 is an exploded perspective view of a multi-conductor differential and
20 common mode filter for use in connector applications;

FIG. 5 shows schematic representations of the differential and common mode filter and prior art filters with FIG. 5a being a multi-capacitor component as found in the prior art and FIG. 5b being the electrical representation of the physical embodiment of the

differential and common mode filter of FIG. 4;

FIG. 6 is a top plan view of the plurality of common ground conductive and electrode plates which make up a high density multi-conductor differential and common filter embodiment;

5 FIG. 6A is a top plan view of the plurality of common ground conductive and electrode plates which make up an alternate high density multi-conductor filter as shown in FIG. 6;

FIG. 7 is a front elevational view of an electrode plate where FIG. 7a and FIG. 7b are the front and back, respectfully, of the electrode plate;

10 FIG. 8 shows a side elevational view of an alternative embodiment of the differential and common mode filter of FIG. 1 which employs the electrode plates of FIG. 7;

FIG. 9 shows a front elevational view of the filter of FIG. 8;

15 FIG. 10 shows a surface mount chip embodiment of a differential and common mode filter with FIG. 10a being a perspective view and FIG. 10b showing an exploded perspective view of the same;

FIG. 11 shows a further embodiment of the filter shown in FIG. 10 with FIG. 11a showing a perspective view in cut away of the filter and FIG. 11b showing a schematic representation of the same;

20 FIG. 12 shows a multi-filter surface mount component with FIG. 12a being a top plan view of the filter; FIGS. 12b through 12d shows top plan views of internal electrode layers; and FIG. 12e shows a front elevational view in cross section of the filter shown in FIG. 12a;

FIG. 13 is not included;

FIG. 14 is an exploded perspective view of the individual film plates which comprise a further embodiment of a differential and common mode filter;

FIG. 15 shows a front elevational view in cross-section of the film plates of FIG.

5 14 in operable cooperation;

FIG. 16 shows a further alternative embodiment of the differential and common mode filter configured primarily for use with electric motors; FIG. 16a shows a top plan view of the motor filter embodiment; FIG. 16b shows a side elevational view of the same; FIG. 16c shows a side elevational view in cross-section of the same; and FIG. 16d is an
10 electrical representation of the physical embodiment of the filter shown in FIG. 16a;

FIG. 17 shows the motor differential and common mode filter embodiment electrically and physically coupled to an electric motor; FIG. 17a shows a top plan view of the filter coupled to a motor and FIG. 17b shows a side elevational view of the same;

FIG. 18 is a logarithmic graph showing a comparison of the emission levels in
15 dBuV/m as a function of frequency for an electric motor with a standard filter and an electric motor with the differential and common mode filter of FIG. 17;

FIG. 19 shows a further alternate embodiment of the motor differential and common mode filter: FIG. 19a shows a top plan view of the plurality of electrode plates; FIG. 19b shows an exploded perspective view of the electrode plates electrically coupled
20 to a plurality of electrical conductors; and FIG. 19c is an electrical representation of the physical embodiment of the motor differential and common mode filter;

FIG. 20 shows a high power embodiment of the differential and common mode filter with FIG. 20a being a schematic representation of the filter and FIG. 20b being a

partial schematic/block diagram of the same;

FIG. 21 shows a high power differential and common mode filter with FIG. 21a being a partially assembled perspective view and FIG. 21b being a schematic representation of the same;

5 FIG. 22 shows a further alternate embodiment of the present invention; Fig. 22a is an exploded prospective view of an alternate multi-conductor differential and common mode filter for use in connector applications; Fig. 22b is a front elevational view of the filter shown in Fig. 22a; Fig. 22c is an electrical representation of the physical embodiment of the filter shown in Fig. 22a; and Fig. 22d is an alternate electrical
10 representation of the physical embodiment of the filter shown in Fig. 22a;

FIG. 23 discloses one application of the filters of the present invention with Fig. 23a being an electrical representation of the physical embodiment of independent surge and electro-magnetic interference (EMI) devices in combination as shown in Fig. 23b;

FIG. 24 discloses a further application of the filters of the present invention with
15 Fig. 24a being an electrical representation of the physical embodiment of a surge protection device in combination with a capacitor as shown in Fig. 24b;

FIG. 25 discloses another application of the filters of the present invention with Fig. 25a being the physical embodiment of a differential and common mode thru-hole filter in combination with a plurality of surge protection devices and Fig. 25b being an
20 electrical representation of the combination shown in Fig. 25a;

FIG. 26 is an elevational view of an alternate embodiment of an electrode plate where Figs. 26a and 26c are the front and back, respectively, of the electrode plate and Fig. 26b is a side elevational view in cross section of the same electrode plate;

FIG. 27 is a side elevational view in cross section of an application in which two electrode plates, as shown in Fig. 26, are employed in an electronic circuit;

FIG. 28 is a side elevational view in cross section of a further application in which two electrode plates, as shown in Fig. 26, and a ground plane are employed in an
5 electronic circuit;

FIG. 29 is an exploded view of the individual internal layers which makeup a multi-component strip filter wherein each internal layer shown is a bottom plan view of the layer; FIG. 30 shows the multi-component strip filter shown in Fig. 29, where
10 Figure 30a is a top plan view, Figure 30b is front side elevational view, Figure 30c is a back side elevational view and Figure 30d is a bottom plan view;

FIG. 31 is an exploded view of the individual internal layers which makeup an alternative multi-component strip filter wherein each internal layer shown is a bottom plan view of the layer;

FIG. 32 is an exploded view of the individual internal layers which makeup an
15 alternative multi-component strip filter wherein each internal layer shown is a bottom plan view of the layer;

FIG. 33 shows the multi-component strip filter shown in Fig. 32, where Fig. 33a is a top plan view, Fig. 33b is front side elevational view, Fig. 33c is a back side elevational view, Fig. 33d is a bottom plan view and Fig. 33e is an end elevational view;

20 FIG. 34 is an exploded view of the individual internal layers which makeup an alternative multi-component strip filter wherein each internal layer shown is a bottom plan view of the layer;

FIG. 35 shows the multi-component strip filter shown in Fig. 34, where Fig. 35a is

a top plan view, Fig. 35b is front side elevational view, Fig. 35c is a back side elevational view, Fig. 35d is a bottom plan view and Fig. 35e is an end elevational view;

FIG. 36 is an exploded view of the individual internal layers which makeup an alternative multi-component strip filter wherein each internal layer shown is a bottom plan view of the layer;

FIG. 37 shows the multi-component strip filter shown in Fig. 36, where Fig. 37a is a top plan view, Fig. 37b is front side elevational view, Fig. 37c is a back side elevational view, Fig. 37d is a bottom plan view and Fig. 37e is an end elevational view;

FIG. 38 is an exploded view of the individual internal layers which makeup multi-component filter wherein each internal layer shown is a bottom plan view of the layer;

FIG. 39 is a schematic representation of the multi-component filter shown in Fig. 38;

FIG. 40 is an isometric view of the multi-component filter shown in Fig. 38 where Fig. 40a is a top plan view of the filter, Fig. 40b is a front elevational view of the filter and Fig. 40c is a side elevational view of the filter;

FIG. 41 shows a further embodiment of the multi-component filter shown in Fig. 38 with additional ground planes for improved performance where Fig. 41A is an exploded view of the individual internal layers of the multi-component filter, Fig. 41B is a schematic representation of the multi-component filter, Fig. 41C is a chart of attenuation values of the multi-component filter at various test frequencies and Fig. 41D is a graphical representation of the attenuation values of the multi-component filter at the various test frequencies listed in Fig. 41C; and

FIG. 42 shows a further application of a surface mount chip embodiment of a

differential and common mode filter where Fig. 42A is a perspective view of the further application which consists of a phase T network integrated passive filter partially exploded and Fig. 42B is a schematic representation of the phase T network integrated passive filter.

5 Detailed Description of the Preferred Embodiment

Due to the continued and increasing use of electronics in daily life and the amount of electromagnetic interference (EMI) and emissions generated, new world electromagnetic compatibility (EMC) requirements are being specified daily for use in such diverse digital and analog applications as in the home, hospitals, automotive, aircraft
10 and satellite industries. The present invention is directed towards a physical architecture for an electronic component which provides EMI suppression, broad band I/O-line filtering, EMI decoupling noise reduction and surge protection in one assembly.

To propagate electromagnetic energy two fields are required, an electric and magnetic. Electric fields couple energy into circuits through the voltage differential
15 between two or more points. Magnetic fields couple energy into circuits through inductive coupling. Magnetic fields originate from currents flowing in a path which could simply consist of a loop of wire. In such loops both fields exist and are also included within circuit traces found on printed circuit boards. These fields start to diverge at frequencies above 1 MHz.

20 As previously noted, propagated electromagnetic energy is the cross product of both electric and magnetic fields. Typically, emphasis is placed on filtering EMI from circuit conductors carrying DC to high frequency noise. This can be explained for two reasons, the first being that a changing electric field in free space gives rise to a magnetic

field and second because a time varying magnetic flux will give rise to an electric field. As a result a purely electric or magnetic time varying field cannot exist. Fields may be primarily electric or primarily magnetic but neither can be generated exclusively.

The main cause of radiated emission problems are due to the two types of
5 conducted currents, differential and common mode. The fields generated by these currents result in EMI emissions. Differential mode (DM) currents are those currents which flow in a circular path in wires, circuit board traces and other conductors in a manner in which the field related to these currents originates from the loop defined by the conductors.

10 Common and differential mode currents differ in that they flow in different circuit paths. Common mode noise currents are surface phenomena relative to ground and, for example, travel on the outer skin of cables which are often grounded to the chassis. To reduce, minimize or suppress the noise it is necessary to provide a low impedance path to ground while simultaneously shortening the overall noise current loop.

15 Turning now to FIG. 1, an exploded perspective view of differential and common mode filter 10's physical architecture is shown. Filter 10 is comprised of a plurality of common ground conductive plates 14 at least two electrode plates 16a and 16b where each electrode plate 16 is sandwiched between two common ground conductive plates 14. At least one pair of electrical conductors 12a and 12b is disposed through insulating
20 apertures 18 or coupling apertures 20 of the plurality of common ground conductive plates 14 and electrode plates 16a and 16b with electrical conductors 12a and 12b also being selectively connected to coupling apertures 20 of electrode plates 16a and 16b. Common ground conductive plates 14 consist entirely of a conductive material such as

metal in the preferred embodiment. At least one pair of insulating apertures 18 are disposed through each common ground conductive plate 14 to allow electrical conductors 12 to pass through while maintaining electrical isolation between common ground conductive plates 14 and electrical conductors 12. The plurality of common ground conductive plates 14 may optionally be equipped with fastening apertures 22 arranged in a predetermined and matching position to enable each of the plurality of common ground conductive plates 14 to be coupled securely to one another through standard fastening means such as screws and bolts. Fastening apertures 22 may also be used to secure differential and common mode filter 10 to another surface such as an enclosure or chassis of the electronic device filter 10 is being used in conjunction with.

Electrode plates 16a and 16b are similar to common ground conductive plates 14 in that they are comprised of a conductive material and have electrical conductors 12a and 12b disposed through apertures. Unlike common ground conductive plates 14, electrode plates 16a and 16b are selectively electrically connected to one of the two electrical conductors 12. While electrode plates 16, as shown in FIG. 1, are depicted as smaller than common ground conductive plates 14 this is not required but in this configuration has been done to prevent electrode plates 16 from interfering with the physical coupling means of fastening apertures 22.

Electrical conductors 12 provide a current path which flows in the direction indicated by the arrows positioned at either end of the electrical conductors 12 as shown in FIG. 1. Electrical conductor 12a represents an electrical signal conveyance path and electrical conductor 12b represents the signal return path. While only one pair of electrical conductors 12a and 12b is shown, Applicant contemplates differential and

common mode filter 10 being configured to provide filtering for a plurality of pairs of electrical conductors creating a high density multi-conductor differential and common mode filter.

The final element which makes up differential and common mode filter 10 is material 28 which has one or a number of electrical properties and surrounds the center common ground conductive plate 14, both electrode plates 16a and 16b and the portions of electrical conductors 12a and 12b passing between the two outer common ground conductive plates 14 in a manner which completely isolates all of the plates and conductors from one another except for the connection created by the conductors 12a and 12b and coupling aperture 20. The electrical characteristics of differential and common mode filter 10 are determined by the selection of material 28. If a dielectric material is chosen filter 10 will have primarily capacitive characteristics. Material 28 may also be a metal oxide varistor material which will provide capacitive and surge protection characteristics. Other materials such as ferrites and sintered polycrystalline may be used wherein ferrite materials provide an inherent inductance along with surge protection characteristics in addition to the improved common mode noise cancellation that results from the mutual coupling cancellation effect. The sintered polycrystalline material provides conductive, dielectric, and magnetic properties. Sintered polycrystalline is described in detail in U.S. Patent Number 5,500,629 which is herein incorporated by reference.

An additional material that may be used is a composite of high permittivity ferroelectric material and a high permeability ferromagnetic material as disclosed in U.S. Patent No. 5,512,196 which is incorporated by reference herein. Such a ferroelectric-

ferromagnetic composite material can be formed as a compact unitary element which singularly exhibits both inductive and capacitive properties so as to act as an LC-type electrical filter. The compactness, formability and filtering capability of such an element is useful for suppressing electromagnetic interference. In one embodiment the

5 ferroelectric material is barium titanate and the ferromagnetic material is a ferrite material such as one based upon a copper zinc ferrite. The capacitive and inductive characteristics of the ferroelectric-ferromagnetic composites exhibit attenuation capabilities which show no signs of leveling off at frequencies as high as 1 Ghz. The geometry of the ferroelectric-ferromagnetic composite will significantly effect the ultimate capacitive and
10 inductive nature of an electrical filter that employs such a composite. The composite can be adjusted during its manufacturing process to enable the particular properties of a filter to be tuned to produce suitable attenuation for specific applications and environments.

Still referring to FIG. 1, the physical relationship of common ground conductive plates 14, electrode plates 16a and 16b, electrical conductors 12a and 12b and material 28
15 will now be described in more detail. The starting point is center common ground conductive plate 14. Center plate 14 has the pair of electrical conductors 12 disposed through their respective insulating apertures 18 which maintain electrical isolation between common ground conductive plate 14 and both electrical conductors 12a and 12b. On either side, both above and below, of center common ground conductive plate 14 are
20 electrode plates 16a and 16b each having the pair of electrical conductors 12a and 12b disposed there through. Unlike center common ground conductive plate 14, only one electrical conductor, 12a or 12b, is isolated from each electrode plate, 16a or 16b, by an insulating aperture 18. One of the pair of electrical conductors, 12a or 12b, is electrically

coupled to the associated electrode plate 16a or 16b respectively through coupling aperture 20. Coupling aperture 20 interfaces with one of the pair of electrical conductors 12 through a standard connection such as a solder weld, a resistive fit or any other method which will provide a solid and secure electrical connection. For differential and common mode filter 10 to function properly, upper electrode plate 16a must be electrically coupled to the opposite electrical conductor 12a than that to which lower electrode plate 16b is electrically coupled, that being electrical conductor 12b. Differential and common mode filter 10 optionally comprises a plurality of outer common ground conductive plates 14. These outer common ground conductive plates 14 provide a significantly larger ground plane which helps with attenuation of radiated electromagnetic emissions and provides a greater surface area in which to dissipate over voltages and surges. This is particularly true when plurality of common ground conductive plates 14 are not electrically coupled to circuit or earth ground but are relied upon to provide an inherent ground. As mentioned earlier, inserted and maintained between common ground conductive plates 14 and both electrode plates 16a and 16b is material 28 which can be one or more of a plurality of materials having different electrical characteristics.

FIG. 1A shows an alternative embodiment of filter 10 which includes additional means of coupling electrical conductors or circuit board connections to filter 10. Essentially, the plurality of common ground conductive plates 14 are electrically connected to an outer edge conductive band or surface 14a. Also each electrode plate 16a and 16b has its own outer edge conductive band or surface, 40a and 40b respectively. To provide electrical connections between electrode plate 16a and 16b and their respective conductive band 40a and 40b while at the same time maintaining electrical isolation

between other portions of filter 10, each electrode plate 16 is elongated and positioned such that the elongated portion of electrode plate 16a is directed opposite of the direction electrode plate 16b is directed. The elongated portions of electrode plates 16 also extend beyond the distance in which the plurality of common ground conductive plates 14 extend with the additional distance isolated from outer edge conductive bands 40a and 40b by additional material 28. Electrical connection between each of the bands and their associated plates is accomplished through physical contact between each band and its associated common ground conductive or electrode plate.

FIG. 2 shows two representations of differential and common mode filter 10. FIG 2a is a schematic representation demonstrating that filter 10 provides a line-to-line capacitor 30 between and coupled to electrical conductors 12a and 12b and two line-to-ground capacitors 32 each coupled between one of the pair of the electrical conductors 12 and inherent ground 34. Also shown in dashed lines is inductance 36 which is provided if material 28 is comprised of a ferrite material, as described in more detail later.

FIG. 2b shows a quasi-schematic of the physical embodiment of filter 10 and how it correlates with the capacitive components shown in FIG. 2a. Line-to-line capacitor 30 is comprised of electrode plates 16a and 16b where electrode plate 16a is coupled to one of the pair of electrical conductors 12a with the other electrode plate 16b being coupled to the opposite electrical conductor 12b thereby providing the two parallel plates necessary to form a capacitor. Center common ground conductive plate 14 acts as inherent ground 34 and also serves as one of the two parallel plates for each line-to-ground capacitor 32.

The second parallel plate required for each line-to-ground capacitor 32 is supplied by the corresponding electrode plate 16. By carefully referencing FIG. 1 and FIG. 2b, the

capacitive plate relationships will become apparent. By isolating center common ground
conductive plate 14 from each electrode plate 16a or 16b with material 28 having
electrical properties, the result is a capacitive network having a common mode bypass
capacitor 30 extending between electrical conductors 12a and 12b and line-to-ground
5 decoupling capacitors 32 coupled from each electrical conductor 12a and 12b to inherent
ground 34.

Inherent ground 34 will be described in more detail later but for the time being it
may be more intuitive to assume that it is equivalent to earth or circuit ground. To couple
inherent ground 34, which center and additional common ground conductive plates 14
10 form, one or more of common ground conductive plates 14 are coupled to circuit or earth
ground by common means such as a soldering or mounting screws inserted through
fastening apertures 22 which are then coupled to an enclosure or grounded chassis of an
electrical device. While differential and common mode filter 10 works equally well with
inherent ground 34 coupled to earth or circuit ground, one advantage of filter 10's
15 physical architecture is that a physical grounding connection is unnecessary.

Referring again to FIG.1 an additional feature of differential and common mode
filter 10 is demonstrated by clockwise and counterclockwise flux fields, 24 and 26
respectively. The direction of the individual flux fields is determined and may be mapped
by applying Ampere's Law and using the right hand rule. In doing so an individual
20 places their thumb parallel to and pointed in the direction of current flow through
electrical conductors 12a or 12b as indicated by the arrows at either ends of the
conductors. Once the thumb is pointed in the same direction as the current flow, the
direction in which the remaining fingers on the person's hand curve indicates the

direction of rotation for the flux fields. Because electrical conductors 12a and 12b are positioned next to one another and represent a single current loop as found in many I/O and data line configurations, the currents entering and leaving differential and common mode filter 10 are opposed thereby creating opposed flux fields which cancel each other and minimize inductance. Low inductance is advantageous in modern I/O and high speed data lines as the increased switching speeds and fast pulse rise times of modern equipment create unacceptable voltage spikes which can only be managed by low inductance surge devices.

It should also be evident that labor intensive aspects of using differential and common mode filter 10 as compared to combining discrete components found in the prior art provides an easy and cost effective method of manufacturing. Because connections only need to be made to either ends of electrical conductors 12 to provide a differential mode coupling capacitor and two common mode decoupling capacitors, time and space are saved.

FIG. 3 shows a comparison of the change in insertion loss relative to frequency of several chip capacitors of the prior art versus differential and common mode filter 10 of the present invention. The graph shows that chip capacitor 50 configured line-to-line with a value of 82 pF or chip capacitor 56 having a value of 82 pF but configured line-to-ground, both demonstrate varying non-linear characteristics. On the other hand filter 10 configured in any of the following ways demonstrates significantly lower linear insertion losses even up to frequencies of 100 MHz: (1) with line-to-line capacitor 54 having a value of 82 pF as compared to conventional capacitor 50 having the same value; (2) with line-to-ground capacitor 58 having a value of 82 pF as compared to conventional capacitor 56 having the same value; and (3) line-to-ground capacitor 52 having a value of

41 pF as compared to both conventional capacitors 50 and 56.

An alternate embodiment of the present invention is differential and common mode multi-conductor filter 110 shown in FIG. 4. Filter 110 is similar to filter 10 of FIGS. 1 and 1A in that it is comprised of a plurality of common ground conductive plates 112 and a plurality of conductive electrodes 118a thru 118h to form differential mode coupling capacitors and common mode decoupling capacitor arrangements which act on a plurality of pairs of electrical conductors, not shown in FIG.4 but similar to electrical conductors 12a and 12b shown in FIGS. 1 and 1A. As described earlier for the single pair conductor filter 10 shown in FIG. 1, common ground conductive plates 112, conductive electrodes 118 and the plurality of electrical conductors are isolated from one another by a pre-selected material 122 having predetermined electrical characteristics such as dielectric material, ferrite material, MOV-type material and sintered polycrystalline material. Each of the plurality of common ground conductive plates 112 has a plurality of insulating apertures 114 in which electrical conductors pass while maintaining electrical isolation from the respective common ground conductive plates 112. To accommodate a plurality of electrical conductor pairs, differential and common mode filter 110 must employ a modified version of the electrode plates described in FIGS. 1 and 1A.

To provide multiple independent conductive electrodes for each pair of electrical conductors, a support material 116 comprised of one of the materials 122 containing desired electrical properties is used. Support plate 116a is comprised of a plurality of conductive electrodes 118b, 118c, 118e and 118h printed upon one side of plate 116a with one coupling aperture 120 per electrode. Support plate 116b is also comprised of a plurality of conductive electrodes 118a, 118d, 118f and 118g printed upon one side of plate 116b. Support plates 116a and 116b are separated and surrounded by a plurality of

common ground conductive plates 112. The pairs of incoming electrical conductors each have a corresponding electrode pair within filter 110. Although not shown, the electrical conductors pass through the common ground conductive plates 112 and the respective conductive electrodes. Connections are either made or not made through the selection of
5 coupling apertures 120 and insulating apertures 114. The common ground conductive plates 112 in cooperation with conductive electrodes 118a thru 118h perform essentially the same function as electrode plates 16a and 16b of FIGS. 1 and 1A.

FIG. 5 shows schematic diagrams of prior art multi-capacitor components and differential and common mode multi-conductor filter 110 of the present invention. FIG.
10 5a is a schematic of prior art capacitor array 130. Essentially, a plurality of capacitors 132 are formed and coupled to one another to provide common ground 136 for array 130 with open terminals 134 provided for connecting electrical conductors to each capacitor 132. These prior art capacitor arrays only allowed common mode decoupling of individual electrical conductors when open terminal 134 of each capacitor 132 was
15 electrically connected to individual electrical conductors.

FIG. 5b shows a schematic representation of differential and common mode multi-conductor filter 110 having four differential and common mode filter pin pair pack arrangements. The horizontal line extending through each pair of electrodes represents the common ground conductive plates 112 with the lines encircling the pairs being the
20 isolation bars 112a. The isolation bars 112a are electrically coupled to common ground conductive plates 112 providing an inherent ground grid separating each of the electrode plates 118a through 118h from one another. The corresponding conductive electrodes 118a thru 118h positioned on support material plates 116a and 116b, both above and below the center common ground conductive plate 112, and form line-to-ground common

mode decoupling capacitors. Each plate, common ground plates 112 and support material plates 116a and 116b, is separated from the others by dielectric material 122. When filter 110 is connected to paired electrical conductors via coupling apertures 120 such as those found in electrode plates 118a and 118c, filter 110 forms a line-to-line differential mode
5 filtering capacitor.

Again referring to FIG. 4, multi-conductor filter 110 is shown having not only a center common ground conductive plate 112 but outer common ground conductive plates 112. As described in relation to FIGS. 1 and 1A these outer common ground conductive plates 112 provide a significantly larger ground plane for filter 110 which helps with
10 attenuation of radiated electromagnetic emissions, provides a greater surface area to dissipate and/or absorb over voltages, surges and noise, and effectively acts as a Faraday shield. This is particularly true when plurality of common ground conductive plates 112 are not electrically connected to circuit or earth ground but are instead relied upon to provide an inherent ground.

15 A further variation of the present invention is differential and common mode multi-conductor filter 680 shown in Fig. 22. Filter 680 has been optimized for use with computer and telecommunications equipment and in particular has been configured for use with RJ 45 connectors. To obtain improved filters performance, filter 680 includes built in chassis and circuit board low frequency noise blocking capacitors in addition to a
20 plurality of differential and common mode filters. As shown in Fig. 22a, the physical construction of filter 680 is substantially similar to filter 110, shown in Fig. 4, and is comprised of a plurality of common ground conductive plates 112, first and second electrode plates 676 and 678 having a plurality of conductive electrodes to form multiple differential and common mode filters including chassis and board blocking capacitors.

As described for earlier embodiments, common ground conductive plates 112, conductive electrodes 686, 688, 690 and 692, blocking electrodes 682 and 684, and the electrical conductors (not shown) which pass through the various plates are all isolated from one another by material 122. To realize particular predetermined electrical characteristics in filter 680, as in all other embodiments of the present invention, material 122 can consist of dielectrics, ferrites, MOV-type material or sintered polycrystalline. Each common ground conductive plate 112 includes a plurality of insulating apertures 114 in which electrical conductors pass while maintaining electrical isolation from common ground conductive plate 112. To obtain the additional chassis and board noise blocking capacitors, filter 680 employs a modified version of the electrode plates of Fig. 1.

As described for Fig. 4, to provide multiple independent components for a number of pairs of electrical conductors, material 122 also serves as support material 116 which is used to fabricate first and second electrode plates 676 and 678. First electrode plate 676 is made up of first and second conductive electrodes 682 and 686 and blocking electrode 688, all printed upon one side of support material 116. Second electrode plate 678 is made up of first and second conductive electrodes 684 and 690 and blocking electrode 692, again printed upon one side of support material 116. First and second electrode plates 676 and 678 are then separated and surrounded by common ground conductive plates 112. What differs in filter 680 from previous embodiments which allows for the combination of differential and common mode filters with built in chassis and board noise blocking capacitors is the configuration of first and second conductive electrodes and blocking electrodes on first and second electrode plates 676 and 678. First and second conductive electrodes 686 and 688 of first electrode plate 676 each include one coupling aperture 120 disposed in the electrode. Blocking electrode 682 is formed to partially

surround first and second conductive electrodes 686 and 688 and includes a plurality of insulating apertures 114 and coupling apertures 120. Second electrode plate 678 is identical to first electrode plate 676 with first and second conductive electrodes 690 and 692 corresponding to first and second conductive electrodes 686 and 688 and blocking electrode 684 corresponding with blocking electrode 682. As is clearly shown in Fig. 22a, when coupled between the various common ground conductive plates 112, first and second electrode plates 676 and 678 are arranged in opposite directions from one another. This particular alignment of first and second electrode plates 676 and 678 allows filter 680 to have a traditional RJ 45 pinout configuration when used in a connector application.

It should be noted that Applicant contemplates other configurations of conductive and blocking electrodes depending upon the desired pinout or wiring arrangement desired and the inverted arrangement of first and second electrode plates 676 and 678 is not required.

As in other embodiments, a number of electrical conductors will pass through common ground conductive plates 112 and first and second electrode plates 676 and 678.

Although the electrical conductors are absent, Fig. 22b shows that this particular embodiment of filter 680 is adapted to accept eight conductors in accordance with RJ 45 connector standards. The interaction of the various conductive electrodes within filter 680 will now be described by referring Figs. 22a through 22d with Fig. 22b included to further correlate the electrical representation with the physical embodiment of filter 680.

Fig. 22d is an alternate electrical representation of filter 680 which should also be referred to as needed. Signal ground (SG) for filter 680 is provided by the combination of common ground conductive plates 112 which act as an inherent ground. The physical separation of the various conductive electrodes of first and second electrode plates 676 and 678 by the conductive plane of common ground conductive plates 112 provides a

substantial ground plane for filter 680 which inherently acts as a ground and assists with attenuation of radiated electromagnetic admissions, provides a greater surface area to dissipate and/or absorb over voltages, surges and noise, and effectively acts as a Faraday shield protecting the filter from external electrical noise and preventing radiation of the same by filter 680.

Referring to the various electrical conductors (not shown) by the numbers 1 through 8 as shown in Figs. 22b, 22c and 22d, the electrical conductors 3 and 5 are connected through coupling apertures 120 to first and second conductive electrodes 686 and 688 respectively. Electrical conductors 4 and 6 are connected through coupling apertures 120 to conductive electrodes 690 and 692 respectively. Conductors 1 and 7 are connected through coupling apertures 120 to blocking electrode 684 and electrical conductors 2 and 8 are similarly connected through coupling apertures 120 to blocking electrode 682. Referring to Fig. 22d, electrical conductors 3 and 6 are filtered differentially by the interaction of first and second conductive electrodes 686 and 692 which act as opposing plates to form a line-to-line capacitor between electrical conductors 3 and 6. The same electrical conductors each receive common mode filtering through line-to-ground capacitors formed by the interaction of first and second conductive electrodes 686 and 692 with common ground conductive plates 112 which forms line-to-ground capacitors between each electrical conductor and the inherent ground formed by the plurality of common ground conductive plates 112.

The same relationship exists for electrical conductors 4 and 5 which are connected to first and second conductive electrodes 690 and 688 respectively. First and second conductive electrodes 690 and 688 form line-to-line capacitors and each interacts with common ground conductive plates 112 to form individual common mode filter capacitors

for each electrical conductor. In addition to the plurality of differential and common mode filters created by the interaction between the various conductive electrodes and common ground conductive plates, chassis and board noise blocking capacitors are also formed by the interaction of common ground conductive plates 112 and blocking electrodes 682 and 684. For instance, chassis ground is connected to the electrical conductors 1 and 7, both of which are electrically connected through coupling apertures 120 to blocking electrode 682 thereby forming one plate of the noise blocking capacitors. The other plate of the noise blocking capacitors is formed by common ground conductive plates 112 which interact with blocking electrode 682. Although interchangeable, electrical conductors 2 and 8 also provide board noise blocking capacitors formed by the interaction of common ground conductive plates 112 and blocking electrode 682. Both the chassis and board blocking noise capacitors allow the inherent ground formed by common ground conductive plates 112 to be capacitively decoupled thereby blocking low frequency electrical noise from the signal carrying conductors. This improves differential and common mode filter performance by essentially electrically cleansing the inherent ground formed by common ground conductive plates 112.

FIG. 6 illustrates a further embodiment of the present invention which provides input/output data line pair filtering for a large number of electrical conductor pairs typical of today's high density information and data buses. Differential and common mode high density filter 150 is comprised of a plurality of common ground conductive plates 112 containing a plurality of insulating apertures 114 and conductive electrode plates 116a and 116b each having electrode patterns 118, insulating apertures 114 and coupling apertures 120. The stacking sequence is reflected in FIG. 6 recognizing that dielectric material will surround each of the individual plates as described for previous

embodiments.

FIG. 6A presents an alternative approach in which differential and common mode high density filter 150 utilizes a tri-coupling of the electrodes to develop a higher capacitance to ground and line-to-line. Again, filter 150 is comprised of a plurality of common ground conductive plates 112 each having a plurality of insulating apertures 114, 5 conductive electrode plates 119a thru 119c with their respective electrode patterns 117a thru 117c. Each conductive electrode plate, 119a through 119c, contains a plurality of insulating apertures 114 and coupling apertures 120 in predetermined positions to allow pairs of electrical conductors to pass through while selectively coupling the electrical 10 conductors to create the desired filter architecture. The stacking sequence of the plates shown in FIG. 6A is again similar to those shown for FIGS. 1, 1A, 4 and 6 and again a predetermined dielectric material 122 surrounds each of the individual plates in varying thicknesses.

FIGS. 7, 8 and 9 show single aperture electrode plate 70 and the use of a plurality 15 of such plates in an alternative embodiment of the differential and common mode filter of the present invention. FIG. 7 shows the two sides of electrode plate 70 with FIG. 7a being the front and FIG. 7b being the back. Referring to FIG. 7a, electrode plate 70 is comprised of material 72 having predetermined electrical properties, such as a dielectric or other material as described earlier, where material 72 is molded into a desired shape 20 which in this case is a disk. Aperture 78 is disposed through electrode plate 70 to allow an electrical conductor to pass. The front of electrode plate 70 is partially covered by conductive surface 74 to create isolation band 82 about the outer perimeter of electrode plate 70. Surrounding aperture 78 is solder band 80 which, once heated, will adhere to an electrical conductor disposed through aperture 78 and electrically connect the conductor

to conductive surface 74. Referring now to FIG. 7b, the backside of electrode plate 70 is similar to the front side in that conductive surface 74 is adhered to material 72 in such a fashion as to provide isolation band 82 around its outer perimeter. Differing from the front side, aperture 78 is surrounded by isolation band 76 to prevent any electrical
5 connection between electrical conductors and conductive surface 74 of the backside of electrode plate 70.

FIGS. 8 and 9 demonstrate how multiple electrode plates 70 are used to create differential and common mode filter 90. The construction of filter 90 is similar to previous embodiments in that common ground conductive plate 98 is sandwiched
10 between at least two electrode plates 70 to provide the parallel plate arrangement necessary to form a plurality of capacitive elements. As shown in FIG. 9, one electrode plate 70 is coupled to one side of common ground conductive plate 98 with a second electrode plate 70 being coupled to the opposite side of plate 98 and offset a distance great enough to allow electrical conductors 92a and 92b to pass through one electrode
15 plate 70 without interference from the other electrode plate 70 coupled to the opposite side of common ground conductive plate 98. Although not clearly shown it should be apparent that common ground conductive plate 98 includes apertures in predetermined positions which correspond with the associated apertures of electrode plates 70 to allow electrical conductors 92a and 92b to pass through as shown in FIG. 8.

20 Common ground conductive plate 98 serves as and provides inherent ground 96, which may be connected to earth or signal ground if desired. Fastening apertures 22 allow filter 90 to be mechanically coupled to a structure. One means of physically coupling electrode plate 70 to common ground conductive plate 98 is shown in FIG. 8. Sandwiched between common ground conductive plate 98 and electrode plate 70's

backside is solder weld 84 which when heated adheres to conductive surface 74 of the backside of electrode plate 70 and the corresponding surface of common ground conductive plate 98. When connecting electrode plate 70 to common ground conductive plate 98, electrode plate 70's backside always faces the corresponding side of common ground conductive plate 98. The same mechanical coupling means is used for both electrode plates. Solder band 80 is also shown for each electrode plate 70 which only couples one of the two electrical conductors 92a and 92b, to their respective electrode plates. The arrangement of common ground conductive plate 98 and electrode plates 70 provides line-to-line differential mode filtering between and line-to-ground decoupling for each electrical conductor 92a and 92b. The differential mode filtering is accomplished by conductive surfaces 74 of the front sides of both electrode plates 70 which act as the parallel plates of a capacitor coupled between electrical conductors 92a and 92b or line-to-line. The line-to-ground decoupling is provided by conductive surfaces 74 of each electrode plate 70 acting as one capacitive plate and common ground conductive plate 98 acting as the other parallel capacitive plate. The parallel capacitive plate provided by common ground conductive plate 98, which serves as inherent ground 96, provides the ground decoupling connection for each electrical conductor, 92a and 92b.

Differential and common mode filter 90 shown in FIGS. 8 and 9 is advantageous in that its construction is relatively simple and its voltage and current handling capacities are only limited by its physical structure which may easily be enlarged or reduced depending upon the desired characteristics.

Figs. 26, 27 and 28 disclose double aperture electrode plate 600 and the use of a plurality of such plates in further alternative embodiments of the differential and common mode filters of the present invention. Referring to Fig. 26a, electrode plate 600 is

comprised of material 616 having predetermined electrical properties, with material 616 being molded into a desired shape shown here as being a disk. A first side of double aperture electrode plate 600 is shown in Fig. 26a and includes first and second apertures 602 and 604 each including an isolation band 606 which separates the apertures from first
5 conductive surface 608. A second side of double aperture electrode plate 600 is shown in Fig. 26c and includes first aperture 602 having isolation band 606 and second aperture 604 directly connected to second conductive surface 610 which spans most of the second side of double aperture electrode plate 600, with the exception of isolation band 612 which runs along the outer perimeter of plate 600. Fig. 26b shows first conductive
10 surface 608 is electrically coupled to side conductive surface 614 which encircles double aperture electrode plate 600. Isolation band 612, located along the perimeter of the second side of double aperture electrode plate 600, physically separates and electrically isolates first and second conductive surfaces 608 and 610 from one another.

When two electrical conductors pass through first and second apertures 602 and
15 604, only the electrical conductor passing through aperture 604 will be electrically connected to second conductive surface 610. The function of double aperture electrode plate 600 is identical to single aperture electrode plate 70 shown in Fig. 7 with the only difference being electrode plate 600 does not have to be arranged in an offset manner to allow passage of opposing electrical conductors as was shown and described for Fig. 9.

20 Fig. 27 shows how multiple double aperture electrode plates 600 are used to create differential and common mode filter 626 which is accomplished by electrically connecting two double aperture electrode plates 600 so the first side of each electrode plate 600, shown in Fig. 26a, faces the first side of the opposing electrode plate 600 with first conductive surface 608 of each electrode plate 600 electrically connected through

means known in the art such as solder 622 melted between the two first conductive surfaces 608. Two electrical conductors, 618 and 620, pass through the aligned apertures of each double aperture electrode plate 600 with electrical conductor 618 electrically connected to second conductive surface 610b of electrode plate 600b and electrical

5 conductor 620 electrically connected to second conductive surface 610a of electrode plate 600a. Following the same principles set forth for the differential and common mode architecture of the present invention, first conductive surfaces 608a and 608b form and act as a common ground conductive plate which provides an inherent ground for differential and common mode filter 626. Second conductive surfaces 610a and 610b of each

10 electrode plate 600a and 600b act as the individual conductive electrodes forming two plates which make up a differential capacitor coupled between electrical conductors 618 and 620. Second conductive surfaces 610a and 610b also form common mode decoupling capacitors when taken in conjunction with first conductive surfaces 608a and 608b which act as the inherent ground. One advantage to double aperture electrode plate 600, as

15 compared to the single aperture electrode plate 70 shown in Fig. 7, is that a separate common ground conductive plate is unnecessary. First conductive surfaces 608a and 608b act as and form the common ground conductive plate. If desired, a separate common ground conductive plate 624 having aligned insulated apertures may be positioned between double aperture electrode plates 600a and 600b, as shown in Fig. 28,

20 to provide an enhanced inherent ground with a greater conductive area for distributing electrical noise and heat.

One trend found throughout modern electronic devices is the continuous miniaturization of equipment and the electronic components which make up that equipment. Capacitors, the key component in differential and common mode filter

arrangements, have been no exception and their size has continually decreased to the point where they may be formed in silicon and imbedded within integrated circuits only seen with the use of a microscope. One miniaturized capacitor which has become quite prevalent is the chip capacitor which is significantly smaller than standard through hole or
5 lead capacitors. Chip capacitors employ surface mount technology to physically and electrically connect to electrical conductors and traces found on circuit boards. The versatility of the architecture of the differential and common mode filter of the present invention extends to surface mount technology as shown in FIG. 10. Surface mount differential and common mode filter 400 is shown in FIG. 10a with its internal
10 construction shown in FIG. 10b. Referring to FIG. 10b, common ground conductive plate 412 is sandwiched between first differential plate 410 and second differential plate 414. Common ground conductive plate 412 and first and second differential plates 410 and 414 are each comprised of material 430 having desired electrical properties dependant upon the material chosen. As for all embodiments of the present invention, Applicant
15 contemplates the use of a variety of materials such as but not limited to dielectric material, MOV-type material, ferrite material, film such as Mylar and newer exotic substances such as sintered polycrystalline.

First differential plate 410 includes conductive electrode 416 coupled to the top surface of material 430 in a manner which leaves isolation band 418 surrounding the outer
20 perimeter of first differential plate 410 along three of its four sides. Isolation band 418 is simply a portion along the edge of material 430 that has not been covered by conductive electrode 416. Second differential plate 414 is essentially identical to first differential plate 410 with the exception being its physical orientation with respect to that of first differential plate 410. Second differential plate 414 is comprised of material 430 having

conductive electrode 426 coupled to the top surface of material 430 in such a manner as to leave isolation band 428 surrounding the outer perimeter of second differential plate 414 along three of its four sides. What is important to note about first and second differential plates 410 and 414's physical orientation with respect to one another is that the one side of
5 each plate in which isolation bands 418 and 428 do not circumscribe are arranged 180° apart from one another. This orientation allows each electrical conductor to be coupled to either individual plate 410 or 414 but not both.

Common plate 412 is similar in construction to first and second differential plates 410 and 414 in that it includes material 430 with common conductive electrode 424
10 coupled to its top surface. As can be seen from FIG. 10b, common plate 412 has two isolation bands 420 and 422 positioned at opposite ends. Common plate 412 is aligned in between first and second differential plates 410 and 414 so that isolation bands 420 and 422 are aligned with the ends of first and second differential plates 410 and 414 which do not have isolation bands. All three plates, common plate 412 and first and second
15 differential plates 410 and 414 do not have any type of conductive surface beneath each plate and therefore when the plates are stacked one on top of the other, conductive electrode 426 is isolated from common conductive electrode 424 by the backside of common plate 412. In a similar fashion common conductive electrode 424 is isolated from conductive electrode 416 by the backside of first differential plate 410 which is
20 comprised of material 430.

Referring now to FIG. 10a the construction of surface mount differential and common mode filter 400 will be further described. Once common plate 412 and first and second differential plates 410 and 414 are sandwiched together according to the arrangement shown in FIG. 10b, a means for coupling electrical conductors to the

different electrodes must be included. Electrical conductors are coupled to surface mount differential and common mode filter 400 through first differential conductive band 404 and second differential conductive band 406 which are isolated from common conductive band 402 by isolation bands 408 positioned in between bands 402, 404 and 406.

- 5 Common conductive band 402 and isolation bands 408 extend 360° around the body of filter 400 to provide isolation on all four sides. First and second differential conductive bands 404 and 406 not only extend 360° around filter 400 but also extend to cover ends 432 and 434, respectively.

By referring back and forth between FIGS. 10a and 10b, the coupling between the
10 bands and the plates can be seen. First differential conductive band 404 including end 434 maintains electrical coupling with conductive electrode 416 which does not have isolation band 418 extending to the end of first differential plate 410. Second differential conductive band 406 is electrically isolated from common plate 412 and first differential plate 410 due to isolation band 422 and 428 respectively. In a similar fashion to that just
15 described, second differential conductive band 406 including end 432 is electrically coupled to conductive electrode 426 of second differential plate 414. Due to isolation bands 420 and 418 of common plate 412 and first differential plate 410, second differential conductive band 406 is electrically isolated from first differential plate 410 and common plate 412.

- 20 Electrical coupling of common conductive band 402 to common plate 412 is accomplished by the physical coupling of sides 436 of common conductive band 402 to common conductive electrode 424 which lacks isolation bands along the sides of common plate 412. To maintain electrical isolation of common conductive electrode 424 from first and second differential conductive bands 404 and 406, isolation bands 420 and 422 of

common plate 412 prevent any physical coupling of ends 432 and 434 of first and second differential conductive bands 404 and 406 with common conductive electrode 424.

As with the other embodiments of the differential and common mode filter of the present invention, conductive electrodes 416 and 426 of first and second differential
5 plates 410 and 414 act as a line-to-line differential mode capacitor when electrical conductors are coupled to first and second differential conductive bands 404 and 406. Line-to-ground decoupling capacitors are formed between each conductive electrode, 416 and 426 respectively, and common conductive electrode 424 which provides the inherent ground.

10 FIG. 11 shows surface mount differential and common mode filter 438 which is a further embodiment of the filter shown in FIG. 10. The cutaway perspective view more clearly shows how first and second differential conductive bands 446 and 450, electrically connect to electrode plates 448 and 452. Electrical connection between common conductive band 442 and common ground conductive plates 440 is also shown with the
15 only difference being that common conductive band 442 is not continuous for 360° around the body of surface mount filter 438 as was shown in FIG. 10.

Another striking difference between filter 438 of FIG. 11 and filter 400 of FIG. 10 is that filter 438 is comprised of a plurality of electrode and common ground conductive plates 448, 452, and 440. The advantage to using a plurality of common ground
20 conductive and electrode plates is that greater capacitance values are obtained while keeping the size of surface mount filter 438 to a minimum. Capacitors, like resistors, can be placed in series and in parallel. While the overall resistance of a plurality of resistors in series is the sum of their individual values, the opposite relationship exists for capacitors. To achieve an additive effect capacitors must be placed in parallel with one

another which filter 438 does by having a plurality of plates coupled to first and second differential conductive bands 446 and 450 and common conductive band 442. As in previous embodiments, material 454 having desired electrical properties surrounds and isolates the plurality of electrode plates 448 and 452 and common ground conductive plates 440 from one another while imparting its corresponding electrical properties to the differential and common mode filter arrangement. FIG. 11b shows a schematic equivalent for surface mount differential and common mode filter 438 and the relationship between the plurality of common ground conductive plates 440 and the plurality of electrode plates 448 and 452.

Electrode plates 448 and 452 are each electrically coupled to their respective conductive bands, 450 and 446. Electrical conductors are then coupled to first and second differential conductive bands 446 and 450 with a plurality of electrode plates 448 and 452 acting in parallel to provide one overall capacitive value coupled between the electrical conductors providing line-to-line differential mode coupling. The plurality of common ground conductive plates 440 act in conjunction with electrode plates 448 and 452 to provide line-to-ground decoupling capacitors between each electrical conductor and common conductive band 442. The plurality of common ground conductive plates 440 serve as the inherent ground which also may be connected to signal or earth ground through common conductive band 442. Again, the physical architecture of the present invention allows for numerous variations and by changing the number of plates and/or their sizes, a wide range of capacitive values and filter characteristics may be obtained.

FIG. 12 shows an alternative multi-component surface mount differential and common mode filter which combines two individual filters into one electronic component. It should be understood that any number of individual filters can be

incorporated into a single electronic component and that the invention is not limited to two individual filters. FIG. 12a shows one interconnect arrangement with FIG. 12b through 12e disclosing the internal electrode and common ground conductive layers. First and second differential conductive bands 154 and 156 are coupled to electrode plates 153 and 155 respectively and bands 154' and 156' are similarly coupled to electrode plates 153' and 155'. Multi-component surface mount filter 160 is also comprised of material 166 having predetermined electrical properties, as described previously, disbursed in between the plurality of electrode and common ground conductive layers. Common ground conductive band 164 is electrically connected to common ground conductive plate 163. What should be noted is that not only does Applicant contemplate multiple components within a single electronic package but that the shape and arrangement and/or length and width of first and second differential conductive bands 154 and 156 and common conductive band 164 may be varied to accompany any type of printed circuit board footprint desirable. The conductive and common bands are only required to be electrically coupled to the associated electrode plates and common ground conductive plate 163 while maintaining electrical isolation among one another. The concept disclosed in FIG. 12 could just as easily be extended to incorporate 10, 20 or 100 differential and common mode filters if desired. Multi-component surface mount differential and common mode filter 160 is particularly useful for providing filtering to large data buses typically consisting of 32 or 64 data lines. These data buses handle digital information at extremely high frequencies emitting large amounts of electromagnetic energy and are also extremely susceptible to over currents and voltage surges which can damage circuitry and distort data.

Figs. 23 and 24 disclose applications for the previously described surface mount

filter, shown in Fig. 11, including electrical representations of the applications. Fig. 23 shows the combination of differential and common mode MOV filter 400a coupled in parallel with differential and common mode capacitive filter 400b which provides both differential and common mode surge protection with increased capacitance normally not obtainable with MOV devices alone. Fig. 23b shows filters 400a and 400b physically stacked together such that first differential conductive bands 446a and 446b are electrically coupled to one and another, second differential conductive bands for 450a and 450b are electrically coupled to one and another and common conductive ground bands 442a and 442b are electrically coupled to each another and represented as 443. As the physical construction of filters 400a and 400b are identical, with the exception being the electrical characteristics of the material in each used to separate the various conductive electrodes, isolation bands 444a and 444b of both filters are also aligned. Although not shown, Applicant contemplates components of the present invention that are not physically identical also being stacked or combined dependent upon the particular application in which the components are used. The benefit of the physical configuration of surface mount filters or components of the present invention is that they can be stacked saving space within circuits consistent with the trend in modern electronics of miniaturization.

The result is shown in Fig. 23a where electrical conductors (not shown) would be coupled between first differential conductive bands 446a and 446b and second differential conductive bands 450a and 450b resulting in differential and common mode filtering and surge suppression. This combination improves overall filter response due to the increased capacitance combined with over voltage and surge protection. Fig. 24 shows an alternate application in which surface mount capacitor 720 is coupled between first and second

differential conductive bands 446 and 450 of differential and common mode MOV surge/filter 400a with the resulting electrical representation showing the line-to-line capacitance provided by capacitor 720. This circuit configuration again increases the effective capacitance of differential and common mode MOV surge/filter 400a. As in

5 Fig. 23, electrical conductors (not shown) are coupled between the combination of first differential conductive band 446 and first conductive band 724 and the combination of second differential conductive band 450a and second conductive band 722.

Figs. 38 through 40 takes the component stacking shown in Figs. 23 and 24 one step further by stacking two or more differential and common mode filters within a single component package. Multi-component filter 806, shown in Fig. 38, is configured in the

10 same manner as the numerous other embodiments of the present invention except that the number of plates is doubled, tripled or multiplied by the number of components being stacked within a single component package. Fig. 38 shows the various plates which make up first and second filters 814 and 816 of multi-component filter 806 with the point of

15 division between the two filters shown by dashed line 818. Both the first and second filters 814 and 816 are constructed in a similar manner. Each filter is comprised of a plurality of common ground conductive plates 808 with different first and second electrode plates, 810 and 812 for filter 814 and 811 and 813 for filter 816, sandwiched in between the various common ground conductive plates 808. Each of the common ground

20 conductive plates 808 and the first and second electrode plates, 810 through 813, are imprinted or etched upon a support material having predetermined electrical properties using various techniques known in the art. When the various layers are stacked additional material having predetermined electrical properties (not shown) is disposed between and electrically isolates the various ground and electrode plates from one another.

As shown in Fig. 39, the result of internally stacking first and second filters 814 and 816 is that two or more differential and common mode filters are coupled in parallel. Multi-component filter 806, shown in Figs. 39 and 40, is made up of first and second filters 814 and 816 with the first electrode plates of each filter, 810 and 811, commonly
5 coupled to first differential conductive band 822, the second electrode plates of each filter, 812 and 813, commonly coupled to second differential conductive band 824 and all of the various common ground conductive plates commonly coupled to common ground conductive band 820. Fig. 40 shows an isometric view of a standard surface mount component package in which multi-component filter 806 is enclosed within. The package
10 is covered by insulated outer casing 826 except for the various conductive bands used for electrically coupling filter 806 with external circuitry.

While only two filters are shown internally stacked within a single component package, Applicant contemplates additional components being internally stacked and does not intend to be limited to the embodiment shown in Figs. 38 through 40. One particular
15 application of the internal stacking technology is in the combination of a high capacitance filter coupled with a low capacitance filter which results in a broad band filter having improved filter performance across a broader frequency range. Referring to Fig. 38, first and second differential plates 811 and 813 of second filter 816 include smaller conductive surfaces 830 than the conductive surfaces 828 found in first filter 814. By varying the
20 size of the conductive surfaces of the first and second differential plates, actual capacitance values of the filters can be varied. Multi-component filter 806 is the combination of high capacitance filter 814 and low capacitance filter 816 with the combination providing a single multi-component filter 806 providing the benefits of a high capacitance filter with improved high frequency performance.

Figs. 41A through 41D is an alternate embodiment of the stacked differential and common mode filters in a single component package shown in Figs. 38 through 40.

Multi-component filter 900, shown in Fig. 41A, is configured in the same manner as the stacked differential and common mode filter of Fig. 38 with the addition of additional
5 common ground conductive plates 912. Fig. 41A shows the various metalized layers or plates which make up first and second filters 914 and 916 of multi-component filter 900 with the point of division between the two filters shown by dashed lines 922. Both the first and second filters 914 and 916 are constructed in a similar manner. Each filter is comprised of a plurality of common ground conductive plates 902 with different first and
10 second electrode plates, 904 and 906 for filter 914 and 905 and 907 for filter 916, sandwiched in between the various common ground conductive plates 902. Each of the common ground conductive plates 902 and the first and second electrode plates, 904 through 907, are imprinted or etched upon a support material having predetermined electrical properties using various techniques known in the art. When the various layers
15 are stacked additional material having predetermined electrical properties (not shown) is disposed between and electrically isolates the various ground and electrode plates from one another.

As in previous embodiments and as shown in Fig. 41B, the result of internally stacking first and second filters 914 and 916 is that two or more differential and common
20 mode filters are coupled in parallel. As shown in Fig. 40 for the previous embodiment of multi-component filter 900, filter 900 is made up of first and second filters 914 and 916 with the first electrode plates of each filter, 904 and 905, commonly coupled to first differential conductive band 918, the second electrode plates of each filter, 906 and 907, commonly coupled to second differential conductive band 920 and all of the various

common ground conductive plates commonly coupled to common ground conductive band 924. The various conductive bands are only identified in relation to the schematic representation shown in Fig. 41B. Although not shown again, the surface mount packaging of multi-component filter 900 is identical to that shown in Fig. 40 for filter 806 where first differential conductive band 822 is equivalent to band 918, second differential conductive band 824 is equivalent to band 920 and common ground conductive band 820 is equivalent to band 924.

Figs. 41C and 41D list and graphically represent the attenuation characteristics of both a single differential and common mode filter of the present invention and multi-component filter 900 shown in Figs. 41A and 41B. The first column of the chart in Fig. 41C lists a range of test frequencies from 1 MHZ to 2000 MHZ at which both filters attenuation characteristics were measured. The second and third columns in Fig. 41C represent attenuation measurements taken from the single differential and common mode filter configured rated at 0.1 uF. In Fig. 41A a single 0.1 uF differential and common mode filter is shown at 916. Columns 4 and 5 of Fig. 41C represent the attenuation characteristics of multi-component filter which consists of 0.1 uF filter 916 and 4.8 nF filter 914 stacked and coupled in parallel to form filter 900. The Figures shown within columns 2 thru 5 of Fig. 41C represent attenuation values in decibels. Column 2 is the attenuation characteristic measured from line-to-ground or from X-to-ground as shown in Fig. 41B. Column 3 is the attenuation characteristic measured from X-to-ground when points X and Y of Fig. 41B are shorted. Columns 4 and 5 were measured in the same fashion as columns 2 and 3 with column 4 being line-to-ground and column 5 having points X and Y shorted with the attenuation measured from X or line-to-ground.

Fig. 41D is a graphical representation of the attenuation curves for both filters. As

can be seen from Fig. 41D the result of incorporating additional common ground
conductive plates 912 between first and second filters, 914 and 916, and on the top and
bottom layers of filter 900, is to increase the resonance point of filter 900 to a higher
frequency. The additional isolation provided by the common ground conductive plates
5 912 gives filter 900 improved crosstalk and ground bounce performance while
eliminating additional field fringing between the hot opposite sides of filter 900 from its
ground to any printed circuit boards filter 900 is coupled. The additional common ground
conductive plates 912 provided to the bottom and top layers of filter 900 also maintains
the differential and common mode fields within plates 912 creating a Faraday cage effect.

10 Fig. 25 discloses a further alternate application which combines differential and
common mode filter 10, as shown in Fig. 1, coupled with two MOV electrode plates 700,
one on top 820 of filter 10 and one on bottom 822 of filter 10, to form a filter which
combines differential and common mode surge protection and capacitive filtering as
shown with reference to Fig. 23. The combination as shown in Fig. 25a provides the
15 further advantage of allowing both filter and MOV components to be combined while the
combination allowing for through-hole coupling of electrical conductors 12a and 12b.
The embodiment shown in Fig. 23 did not require separate MOVs because it was
configured for surface mount technology in accordance with the present invention. The
embodiment shown in Fig. 25a is necessary because MOV components having through-
20 hole coupling apertures are generally not available due to the detrimental effect the
apertures have on the overall operating and cost characteristics of the MOVs. To allow
for electrical coupling of MOVs 700 to the electrode plates internal to differential and
common mode filter 10, shown in Fig. 1, several surface modifications to filter 10 are
necessary. The top 820 and bottom 822 of differential and common mode filter 10 have

been modified, as shown in Fig. 25c, to replace one insulating aperture 18 with through-hole plated coupling aperture 718. Through-hole plated coupling aperture 718 of top 820 and bottom 822 are positioned so that each corresponds with opposite electrical conductors 12a or 12b. Although not shown, each through-hole plated coupling aperture

5 718 is electrically connected to one of the two electrode plates embedded within differential and common mode filter 10 thereby allowing electrical connection of electrical conductors 12a and 12b to the respective electrode plates which form a line-to-line differential capacitor between conductors 12a and 12b. To allow for coupling of MOV 700 to the top and bottom of differential and common mode filter 10, through-hole

10 plated coupling aperture 718 includes strip 824 of conductive material to which one of the two contacts of each MOV 700 is electrically connected. Each MOV 700 includes two terminals 828 and 830 to which MOV 700 electrically couples to other circuits. As shown in Fig. 25a, terminals 830 of both MOVs 700 are physically and electrically coupled to conductive surface 826 of differential and common mode filter 10 through

15 standard means such as application of solder 710. Conductive surface 826 of differential and common mode filter 10 is electrically coupled to common ground conductive plates 14 as shown in Fig. 1. Terminals 828 of each MOV 700 are physically and electrically coupled by solder 710 to conductive strip 824 which connects terminals 828 with the respective electrical conductor 12a and 12b which in turn is connected to the internal

20 electrode plates of differential and common mode filter 10. The result is shown in Fig. 25b and consists of the combination of differential and common mode MOV surge protection in parallel with differential and common mode capacitive filtering between terminals 716a and 716b to which electrical conductors 12a and 12b are electrically coupled.

Figs. 29 and 30 show a further alternative multi-component surface mount differential and common mode filter designed to provide a strip of filters for varied use. This specific design is for use with multi conductor electronic connectors. As in other embodiments of the present invention, strip filter 642 is comprised of a plurality of

5 common ground conductive plates 656 with first and second electrode plates 662 and 664 sandwiched in between the various common ground conductive plates 656. Strip filter 642, shown in Fig. 29, has four sets of differential and common mode filters. Each common ground conductive plate 656 is etched upon support material 616 having predetermined electrical properties, as disclosed throughout the specification, so that

10 portions of material 616 act as insulation on either side of each common ground conductive plate 656 with only ground extensions 660 extending to the edges of support material 616. The various first and second electrode plates 662 and 664 are also formed on strips of support material 616 so that each electrode plate is surrounded by material 616 except for electrode extensions 666 which extend to the edges of support material

15 616. As can be seen in Fig. 29, each electrode extension 666 of each first electrode plate 662 extends in an opposite direction from the electrode extension 666 of the corresponding second electrode plate 664. The arrangement of ground extensions 660 and electrode extensions 666 can be reconfigured in numerous patterns as long as a convenient layout for electrical conductor coupling is created. As in the various other

20 embodiments of the present invention, each differential and common mode filter included in strip filter 642 consists of a first and second electrode plate 662 and 664 sandwiched between common ground conductive plates 656 with additional material having predetermined electrical properties (not shown) disposed between and electrically isolating the various ground and electrode plates from one another. Fig. 30 shows top,

bottom and side views of strip filter 642 having first and second differential conductive bands 652 and 654 running perpendicular to the lengths of support material 616 and slightly overlapping onto the top of strip filter 642, as shown in Fig. 30a. The bottom of strip filter 642, as shown in Fig. 30d, is the same as the top to allow for surface mounting

5 of strip filter 642. Common ground conductive bands 650 extend vertically up the ends and onto the top and bottom of strip filter 642, as indicated by the portions labeled 650 in Figs. 30a and 30d. Additional common ground conductive bands 650 are also found on the top and bottom of strip filter 642 but in this configuration they do not extend down the sides. First and second differential conductive bands 652 and 654 extend down the

10 corresponding sides of strip filter 642 allowing the various electrode extensions 666 of each of the first and second electrode plates 662 and 664 to electrically couple to their respective conductive bands thereby allowing connection of external electrical conductors to the various internal electrode plates of strip filter 642. For purposes of clarity, the corresponding first and second electrode plates 662 and 664 and first and second

15 differential conductive bands 652 and 654 include suffix designations (a) through (d) which represents each of the four differential and common mode filters included within strip filter 642. Fig. 31 is a further example of strip filter 642 which includes an additional first electrode plate 662e. By adding an additional electrode plate strip filter 642 can now accommodate an odd number of electrical conductors. An example of an

20 application requiring an odd number of electrical conductors is providing filtering for D-sub connectors which typically have 9 or 15 conductors. While not shown, the only difference in the top, bottom and side views of strip filter 642, shown in Fig. 31, is that an additional conductive band 652 and one or more common ground conductive bands 650

would be added to accomodate the coupling of the additional conductors. By adding first electrode plate 662e without a corresponding second electrode plate, electrode plate 662e forms a line-to-ground capacitor between itself and the plurality of common ground conductive plates 656. Although a corresponding second electrode plate to first electrode plate 662e is missing, differential and common mode filtering still takes place between the electrical conductor that is connected to first electrode plate 662e and any one of the electrical conductors coupled to second electrode plates 664a - d.

Figs. 32 through 37 show a number of variations of the multi-component surface mount differential and common mode strip filters shown in Figs. 29 through 31.

Referring to Figs. 32 and 33, strip filter 800 is comprised of a plurality of common ground conductive plates 656 with first and second electrode plates 662 and 664 sandwiched in between the various common ground conductive plates 656. As in the previous embodiments, strip filter 800 has four pairs of contacts for the same differential and common mode filter, 1A, 4A, 5A and 8A for electrode plate 662 and 2B, 3B, 6B and 7B for electrode plate 664. Each common ground conductive plate 656 is etched upon support material 616 having predetermined electrical properties, as disclosed throughout this specification, so that portions of material 616 act as insulation on either side of each common ground conductive plate 656. Unlike the embodiments shown in Figs. 29 through 31, each of the common ground conductive plates 656 has portions of materials 616 extending lengthwise on either side of common ground conductive plate 656. The first and second electrode plates 662 and 664 are also formed on strips of support material 616 so that the electrode plates are surrounded by material 616 except for electrode extensions 666 which extend to the edges of support material 616. Additional material

having predetermined electrical properties (not shown) is disposed between and electrically isolates the various common ground conductive plates 656 and electrode plates 662 and 664, all from one another. Strip filter 800 is advantageous in that it provides greater connection versatility with low inductance.

5 Fig. 33 shows top, bottom and side views of strip filter 800 having first and second differential conductive bands 652 and 654 running perpendicular to the lengths of support material 616 and slightly overlapping onto the top of strip filter 800, as shown in Fig. 33a. The bottom of strip filter 800, as shown in Fig. 33d, is the same as the top to allow for surface mounting of strip filter 800. Common ground conductive bands 650
10 extend vertically up the ends and onto the top and bottom of strip filter 800, as shown in Figs. 33a, 33d and 33e. First and second differential conductive bands 652 and 654 extend down the corresponding sides of strip filter 800 allowing the various electrode extensions 666 of each of the first and second electrode plates 662 and 664 to electrically couple to their respective conductive bands thereby allowing connection of external
15 electrical conductors to the first and second internal electrode plates.

 Figs. 34 and 35 show a further embodiment of the present invention in strip filter 802 with the only difference being the actual configuration and orientation of the various electrode extensions 666 of each of the first and second electrode plates 662 and 664. As clearly shown in Figs. 32 through 35, the connection or pinout configurations of the strip
20 filters can be arranged to suit any application. Strip filter 804, as shown in Figs. 36 and 37, is a further embodiment which emphasizes the common ground connection. Referring to Fig. 36, each common ground conductive plate 656 is imprinted or etched upon support material 616 having predetermined electrical properties through techniques known in the

art, so that an elongated strip of material 616 acts as insulation along one side of each common ground conductive plate 656. The first and second electrode plates 662 and 664 are essentially the same as in the previous embodiments except that electrode extension 666 of both the first and second electrode plates 662 and 664 extend from the same side of the electrode plates as the insulation strips 616 extend on each the common ground conductive plates 656. Fig. 37 shows top, bottom, side and end views of strip filter 804 having first and second differential conductive bands 652 and 654 running perpendicular to the lengths of support material 616 and slightly overlapping onto the top of strip filter 804, as shown in Fig. 37a. The bottom of strip filter 804, as shown in Fig. 37d, is the same as the top to allow for surface mounting of strip filter 804. In this embodiment, common ground conductive band 650 extends vertically up the ends and onto the top and bottom of strip filter 804 and entirely encompasses one side of strip filter 804, as shown in Fig. 37c. As with the first and second differential conductive bands 652 and 654, the common ground conductive band 650 also extends onto the top and bottom of strip filter 804 along the full length of the covered side. The configuration of strip filter 804 is particularly useful in applications requiring a large ground plane which acts as a shield and is capable of absorbing and dissipating greater amounts of heat and electromagnetic interference.

FIGS. 14 and 15 disclose a further embodiment of a differential and common mode filter formed on a film or Mylar-like medium. This embodiment is comprised of a film medium and consists of a common ground conductive plate 480 followed by the first electrode differential plate 460, then another common ground conductive plate 480 and second electrode differential plate 500, then another common ground conductive plate

480. Each plate is essentially comprised of film 472, which itself may be comprised of a number of materials such as but not limited to Mylar, wherein film 472 is completely metallized on one side creating a metallized plate. Using lasers, portions of metallized material are removed (demetallized) in predetermined patterns to create isolation barriers.

- 5 First differential plate 460 has two laser edged isolation barriers 462 and 466, which divide first differential plate 460 into three conductive areas: electrode 464, isolated electrode 468 and common electrode 470. Second differential plate 500 is identical to first differential plate 460 in that it has two isolation barriers 506 and 504 which divide second differential plate 500 into three conductive areas: electrode 510, isolated electrode
- 10 502 and common electrode 508. For both first and second differential plates 460 and 500, isolation barriers 462 and 506 are essentially U-shaped to create electrodes 464 and 510 which encompass a large area of first and second plates 460 and 500. U-shaped isolation barriers 462 and 506 allow electrode 464 and 510 to extend fully to ends 476 and 514, respectively. Extending from isolation barrier 462 and 506 are members 474 and 512 and
- 15 extending from isolation barriers 466 and 504 are members 473 and 513. Members 474 and 512 extend perpendicular to and outward from the ends of u-shaped isolation barriers 462 and 506 at their points nearest ends 476 and 514 and members 473 and 513 extend perpendicular to and outward from isolation barriers 466 and 504 respectively in order to fully isolate common electrodes 470 and 508 from ends 476 and 514. Also, both first and
- 20 second differential plates 460 and 480 have isolated electrodes 468 and 502 formed on opposite of ends 476 and 514 by isolation barriers 466 and 504.

Common ground conductive plate 480 includes isolation barriers 482 and 492 which divide common ground conductive plate 480 into three conductive surfaces:

common electrode 488, isolated electrode 484 and isolated electrode 494. As shown, isolation barriers 482 and 492 run vertically adjacent to and in parallel with the right and left edges of common ground conductive plate 480. Both isolation barriers 482 and 492 also include members 496 extending outward and perpendicular from the vertical sections of isolation barriers 482 and 492 and are positioned so when plates 460, 480 and 500 are stacked, they are aligned with the horizontal portions of the U-shaped isolation barriers 462 and 506 of first and second differential plates 460 and 500.

An additional feature is that common ground conductive plate 480 can be optimized for use in filtering AC or DC signals. Isolation barriers 492 and 482 as described above are optimized for use in filtering DC signals. For DC operation isolated electrodes 484 and 494 require very little area within common ground conductive plate 480. When the filter is comprised of a film medium and used for filtering AC signals, isolated electrodes 484 and 494 require a greater area which is accomplished by etching modified isolation barriers 486 and 490. The vertically running isolation barriers 484 and 494 are etched closer together and closer to the center of common ground conductive plate 480. To accommodate this modification, members 496 extending outward and perpendicular from the vertical sections are longer than for the DC version. The greater area isolated electrodes 484 and 494 provide better AC filtering characteristics, although either configuration provides filtering to both types of current.

FIG. 15 is a cross-section of film medium differential and common mode filter 540 comprised of a plurality of plates similar to those shown in FIG. 14. As for the surface mount chip embodiment shown in FIG. 11, film differential and common mode filter 540 can also consist of more than five plates in effect coupling capacitors in parallel

to increase overall capacitance.

The top and bottom of filter 540 consist of protective cover layers 555. Situated below the top protective cover layer 555 is common ground conductive plate 480, followed by an electrode plate 460, followed by another common ground conductor plate 480, followed by the next electrode plate 500 and then another common ground conductive plate 480. The previous sequence of alternating ground and electrode plates can be repeated to achieve additional capacitance. Shown in cross section each layer or plate is comprised of a film 558 possessing a conductive metalized upper surface 556 which have isolation patterns cut into the metal surface with a laser creating isolation patterns 554. Terminal conductive blocks 550 and 552 are comprised of pure aluminum which is deposited on the edges and penetrates into the film extensions to provide a highly conductive termination consisting of like metals. The extensions described are created by stacking the different plates in a sequence that has every electrode plate 460 or 500 surrounded by common ground conductive plates 480 as pictured in Fig 15. The electrode plates 460 and 500 are offset from each other and the common ground conductive plates to facilitate edge termination.

FIGS. 16 through 19 are directed towards embodiments of the differential and common mode filter configured and optimized for use with electric motors. Electric motors are a tremendous source of electromagnetic emissions. This fact is evident even to layman, as most people have experienced running a vacuum cleaner in front of an operating television set and noticing "snow" fill the screen. This interference with the television is due to the electromagnetic emissions from the motor. Vacuum cleaners are by no means the only source of electromagnetic emissions. Electric motors are used

extensively in a number of home appliances such as washing machines, dryers, dishwashers, blenders, hair dryers. In addition, most automobiles contain a number of electric motors to control the windshield wipers, electric windows, electric adjustable mirrors, retractable antennas and a whole host of other functions. Due to the prevalence
5 of electric motors and increased electromagnetic emissions standards there is a need for differential and common mode filtering.

Electric motor filter 180 may be made in any number of shapes but in the preferred embodiment shown in FIG. 16 it is essentially a rectangular block comprised of material 182 having one of a number of predetermined electrical properties. FIG. 16a
10 shows the outer construction of filter 180 which consists of a rectangular block of material 182 having an insulated shaft aperture 188 disposed through filter 180's center, conductive bands 184 and 194 and common conductive bands 186. FIG. 16b shows a side view of filter 180 with the arrangement of conductive bands 184 and 194 and common conductive band 186 being electrically and physically isolated from one another
15 by sections of material 182 positioned between the various bands. FIG. 16c shows a cross section along line A of FIG 16a. As in all previous embodiments, the physical architecture of the present invention is comprised of conductive electrodes 181 and 185 with common conductive electrode 183 sandwiched in between. Material 182 having predetermined electrical properties is interspersed between all of the electrodes to prevent
20 electrical connection between the various conductive electrodes 181 and 185 and common conductive electrode 183. Similar to that of the surface mount embodiments of the present invention, filter 180 employs conductive bands 184 and 194 to electrically connect filter 180's internal electrodes to electrical conductors. Conductive electrode 181

extends fully to and comes in contact with conductive band 184 to provide the electrical interface required. As shown in FIG. 16c, conductive electrode 181 does not extend fully to come in contact with conductive band 194 which is coupled to conductive electrode 185. Although not shown, common conductive electrode 183 extends fully between
5 common conductive bands 186 without coming in contact with conductive bands 184 and 194. Again, by coupling common conductive bands 186 to signal or earth ground, a "true" ground may be employed rather than the inherent ground provided by common conductive electrode 183.

FIG. 16d is a schematic representation of differential and common mode electric
10 motor filter 180 showing conductive electrodes 181 and 185 providing the two necessary parallel plates for a line-to-line differential mode coupling capacitor while at the same time working in conjunction with common conductive electrode 183 to provide line-to-ground common mode decoupling capacitors with common conductive electrode 183 acting as the inherent ground. Also shown are conductive bands 184, 194 and common
15 conductive band 186 which allow electric motor filter 180 to be connected to external electrical conductors. While the preferred embodiment of FIG. 16 only shows one common conductive electrode 183 and two conductive electrodes 181 and 185, Applicant contemplates the use of a plurality of electrodes to obtain varying capacitance values through the additive effect of parallel capacitance similar to that described for previous
20 embodiments.

FIG. 17 shows differential and common mode electric motor filter 180 electrically and physically coupled to electric motor 200. As shown in FIG. 17a, electric motor filter 180 is placed on top of electric motor 200 having motor shaft 202 extending outward

therefrom. Motor shaft 202 is disposed through shaft aperture 188 of filter 180 with conductive bands 184 and 194 electrically coupled to connection terminals 196, which are isolated from one another and the rotor of electric motor 200. The individual connection terminals 196, although not shown, are then electrically connected to electrical supply lines providing electric motor 200 with power. Once electric motor filter 180 is connected /coupled to electric motor 200, motor face plate 208 is placed on top of both motor 200 and filter 180 with motor shaft 202 disposed through a similar aperture in the center of motor face plate 208. Face plate 208 is then physically coupled to the body of motor 200 through the use of clamps 206. While not shown, filter 180 may be used with its inherent ground by coupling common conductive bands 186 to the motors enclosure or common conductive bands 186 may be directly wired to circuit or earth ground.

FIG. 18 is a logarithmic graph showing a comparison of electric motor 200's electromagnetic emission levels as a function of frequency with the result of an electric motor having a standard filter being shown at 220 and the results of differential and common mode electric motor filter 180 shown at 222. The graph demonstrates that between 0.01 MHz and approximately 10 MHz there is a minimum of a 20dB suppression of electromagnetic emissions throughout the range with even more pronounced decreases in the 0.1 to 1 MHz range. One can see that at the upper frequency range of 10 - 20 MHz and beyond, the decrease in electromagnetic emissions is not as great as at the lower frequencies but this is not particularly critical as most electric motors operate well below this frequency range thereby allowing electric motor filter 180 to provide enhanced performance with decreased electromagnetic emissions for the majority of applications.

Differential and common mode electric motor filter 230 shown in FIG. 19 is a further embodiment of the filter of FIG. 16. The multi-plate embodiment of FIG. 19 is almost identical to the filter embodiment shown and described in FIG. 1 with the exceptions being the shapes of the plurality of plates and that each plate includes motor shaft aperture 242 to allow the plurality of plates and filter 230 itself to be coupled with the top of an electric motor without interfering with the motor shaft and its rotation. FIG 19a shows the individual plates of filter 230 which include common ground conductive plate 232 and a plurality of conductive plates 246 with all three plates having motor shaft apertures 242. Common ground conductive plate 232 is comprised of a conductive material and in the preferred embodiment is fabricated from a piece of metal. All three plates have at least two apertures 252 which accept electrical conductors 244 as shown in FIG.19b. The two conductive plates 246 of FIG. 19a show opposite sides of plate 246. As in the other embodiments already described, conductive plates 246 are fabricated of material 254 having predetermined electrical properties wherein one side of plate 246 is covered by a conductive surface 236 with the other side of plate 246 having a non-conductive surface 234. To provide electrical coupling between each electrical conductor 244 and the appropriate conductive surface 236 of each conductive plate 246, one of the two apertures 252 is a coupling aperture 240 while the other aperture 252 is surrounded by an insulating ring 238. Both apertures 252 within common ground conductive plate 232 are surrounded by insulating rings 238 to prevent any electrical connection between common ground conductive plate 232 and either electrical conductor 244.

FIG. 19b shows the operative physical coupling of common ground conductive plate 232 and conductive plates 246. Common ground conductive plate 232 is

sandwiched between conductive plates 246 in such a way that non-conductive surface 234 of each conductive plate 246 is facing and comes in contact with one of the two sides of common ground conductive plate 232. Conductive plates 246 are also arranged so that insulating rings 238 of each plate 246 are positioned so only one of the two electrical
5 conductors 244 is coupled to either conductive surface 236 of conductive plates 246. Once common ground conductive plate 232 and the plurality of conductive plates 246 are physically coupled the entire arrangement which makes up differential and common mode electric motor filter 230 is then placed over the top of an electric motor with the motor shaft extending through shaft apertures 242 of each of the plates.

10 FIG. 19c is a schematic representation of the filter components showing how the individual conductive surfaces of the plurality of plates interact to form the line-to-line and line-to-ground capacitors which form filter 230. Because the plurality of conductive plates 246 are essentially identical and are just arranged differently with respect to common ground conductive plate 232, the schematic shown in FIG. 19c uses prime
15 reference numerals to indicate conductive surfaces 236 of the individual conductive plates 246.

FIGS. 20 and 21 show a high-power embodiment of the differential and common mode filter of the present invention. FIG. 20a shows a quasi-schematic representation of the physical arrangement of plates which make up the filter shown in FIG. 20b. Referring
20 to both FIGS. 20a and 20b it can be seen that common ground conductive plate 292 is again sandwiched between two conductive electrode plates, 270 and 270', which are individually connected / coupled to electrical conductors 275a and 275b. Each conductive electrode plate, 270 and 270', consists of a material 264 having specific

predetermined properties, with each plate then having a conductive surface to which electrical connections are made. After electrical conductors 275a and 275b are connected to conductive electrode plates 270 and 270', the conductive surface is coated with insulation. Conductive electrode plates 270 and 270' are physically coupled to common
5 ground conductive plate 292 via typical adhesive material known in the art. A clearer representation of high-power differential and common mode filter 260 is shown in FIG. 21 with FIG. 21a showing the physical embodiment and FIG. 21b showing a representative schematic. Filter 260, as shown in FIG. 21a, is comprised of common ground conductive plate 262 sandwiched between wheels of material 264 having
10 predetermined electrical properties. Wheels 264 of material are held in place by conductive electrodes 270 and 270' with coupling axle 278 disposed through the plurality of apertures 266, not shown, and disposed through wheels 264 and common ground conductive plate 262. To manage the higher current and voltage conditions filter 260 is designed for, common ground conductive plate 262, conductive plates 270 and 270' and
15 wheels of material 264 are typically sized much larger than previous embodiments of the present invention. To allow filter 260 to be connected to external electrical conductors, conductive electrodes 270 have connecting members 284 extending therefrom which are mechanically coupled to connection terminals 275a and 275b through common means such as tightening screws and washers. Connection terminals 275a and 275b are mounted
20 on top of enclosure lid 282 to create a one piece assembly consisting of enclosure lid 282, common ground conductive plate 262, conductive electrodes 270 and 270' and wheels 264 of material. This single component is then placed within component enclosure 276 which has flanges 272 extending from common ground conductive plate 262 coupled to

enclosure mounting holes 280. This arrangement provides a means of coupling the inherent ground provided by common ground conductive plate 262 to circuit or earth ground if desired. FIG. 21b shows the relationship of the different physical components of FIG. 21a that make up filter 260 schematically represented. As in all other

5 embodiments of the present invention, conductive electrodes 270, represented with and without a prime to indicate separate surfaces, make up the two parallel plates necessary for a line-to-line capacitor coupled between connection terminals 274. Conductive electrodes 270 individually but in conjunction with common conductive electrode 262 make up line-to-ground common mode decoupling capacitors with common conductive

10 electrode 262 acting as the inherent ground.

Fig. 42A and 42B show phase T network filter 940 which is a further application of the various surface mount differential and common mode filters disclosed previously. Phase T network filter 940 is comprised of differential and common mode filter 942 having common ground conductive bands 944 and first and second differential conductive

15 bands (not shown) located on either end of differential and common mode filter 942. Coupled to each of the common ground conductive bands 944 are common ground conductive terminals 950 to which solderable connections can be made to desired external circuitry. Coupled to each end of differential and common mode filter 942 are inductive ferrite enclosures 952 and 954 respectively. Each inductive ferrite enclosure, 952 and

20 954, is composed of a solderable ferrite material to which the first and second differential conductive bands (not shown) of differential and common mode filter 942 are soldered internally to their respective inductive ferrite enclosures. Enclosure 954 (as well as 952) includes electrode plate terminals 948 (946) physically coupled to the sides of each

enclosure with a portion disposed through apertures 960 so terminals 946 and 948 make electrical contact with the first and second differential conductive bands of filter 942. This arrangement is better seen from the additional reversed view of enclosure 954 (952) shown in dashed lines at 966. Fig. 42B is a schematic representation of phase T network filter 940 showing multiple inductors 958 coupled to first and second electroplate terminals 946 and 948 of differential and common mode filter 942 thereby creating phase T network filter 940 shown in Fig. 42A.

Phase T network filter 940 is advantageous in high signal current and high frequency noise applications because the present embodiment is capable of shunting noise to ground while allowing high signal current to flow through the terminations of the device with greater noise reduction. First and second electrode plate terminals 946 and 948 provide filter 940 with the high current carrying conductors necessary for such applications and the inductive ferrite enclosures 952 and 954 establish a magnetic field. This combination improves the high frequency filter effectiveness such that the attenuation characteristics of filter 940 approach a slope of 40 - 60dB per decade. Phase T network filter 940 is particularly suited for use in low impedance circuits.

As can be seen, many different applications of the differential and common mode filter architecture are possible and review of several features universal to all the embodiments must be noted. First, the material having predetermined electrical properties may be one of a number in any of the embodiments including but not limited to dielectric material, metal oxide varistor material, ferrite material and other more exotic substances such as Mylar film or sintered polycrystalline. No matter which material is used, the combination of common ground conductive plates and electrode conductive

plates creates a plurality of capacitors to form a line-to-line differential coupling capacitor between and two line-to-ground decoupling capacitors from a pair of electrical conductors. The material having electrical properties will vary the capacitance values and/or add additional features such as over-voltage and surge protection or increased
5 inductance, resistance, or a combination of all the above.

Second, in all embodiments whether shown or not, the number of plates, both common conductive and electrode, can be multiplied to create a number of capacitive elements in parallel which thereby add to create increased capacitance values.

Third, additional common ground conductive plates surrounding the combination
10 of a center conductive plate and a plurality of conductive electrodes may be employed to provide an increased inherent ground and surge dissipation area and a true Faraday shield in all embodiments. Additional common ground conductive plates can be employed with any of the embodiments shown and is fully contemplated by Applicant.

Finally, from a review of the numerous embodiments it should be apparent that
15 the shape, thickness or size may be varied depending on the electrical characteristics desired or upon the application in which the filter is to be used due to the physical architecture derived from the arrangement of common ground conductive and conductive electrode plates.

In fact the differential and common mode filter, although not shown, could easily
20 be fabricated in silicon and directly incorporated into integrated circuits for use in such applications as communication chips. The differential and common mode filter would be embedded and filter communication or data lines directly from their circuit board terminal connections, thus reducing circuit board real estate requirements and further reducing

overall circuit size while having simpler production requirements. Integrated circuits are already being made having capacitors etched within the silicone foundation which allows the architecture of the present invention to readily be incorporated with technology available today.

- 5 Although the principals, preferred embodiments and preferred operation of the present invention have been described in detail herein, this is not to be construed as being limited to the particular illustrative forms disclosed. It will thus become apparent to those skilled in the art that various modifications of the preferred embodiments herein can be made without departing from the spirit or scope of the invention as defined by the
- 10 appended claims.

Claims

What is claimed is:

1. A line conditioning electronic component comprising:

at least one common ground conductive plate having at least two insulating

5 apertures;

at least two electrode plates each having at least one insulating aperture and at least one coupling aperture, wherein said first electrode plate is stacked below said common ground conductive plate and said second electrode plate is stacked above said common ground conductive plate, wherein said at least two electrode plates sandwich
10 said at least one center common ground conductive plate;

at least two electrical conductors disposed through said apertures of said common ground conductive plate and said at least two electrode plates, wherein each of said at least two conductors is electrically connected to a different electrode plate; and

a material having predetermined electrical properties, wherein said material is
15 maintained between said common ground conductive plate and said at least two electrode plates preventing direct electrical connection between said plates creating a capacitive element coupled between said at least two electrical conductors and creating two capacitive elements, one coupled between one electrical conductor and said common ground conductive plate and the other coupled between the other electrical conductor and
20 said common ground conductive plate.

2. A line conditioning electronic component as recited in claim 1, wherein said material having predetermined electrical properties is selected from the group consisting

of dielectric materials, metal oxide varistor materials, ferrite materials, sintered polycrystalline materials and ferroelectric-ferromagnetic composite materials wherein the particular material will determine the specific performance in both filter and surge protection functions.

5

3. A line conditioning electronic component as recited in claim 1, further comprising at least two common ground conductive plates each having at least two insulating apertures, wherein said first common ground conductive plate is stacked below said first electrode plate and said second common ground conductive plate is stacked above said second electrode plate, wherein said material having predetermined electrical properties is maintained between said electrode plates and said at least two common ground conductive plates and wherein said at least two electrical conductors are disposed through said apertures of said first and second common ground conductive plates.

- 15 4. A line conditioning electronic component as recited in claim 1, further comprising a plurality of outer conductive surfaces wherein each of said at least two electrode plates and said common ground conductive plates are individually and independently electrically coupled to separate outer conductive surfaces.

- 20 5. A line conditioning electronic component as recited in claim 1, wherein each of said at least two electrode plates contains a plurality of electrode patterns, each of said electrode patterns having at least one insulating aperture and at least one coupling aperture;

wherein said at least one common ground conductive plate contains two insulating apertures for each of said electrode patterns contained in each of said at least two electrode plates; and

wherein a plurality of electrical conductors are disposed through said apertures
5 with one pair of electrical conductors disposed through each of said electrode patterns creating a capacitive element coupled between each pair of said electrical conductors and creating two capacitive elements each coupled between one of said electrical conductors and said common ground conductive plate.

10 6. A line conditioning electronic component as recited in claim 5, wherein each of said electrode patterns formed on said electrode plates contains at least one coupling aperture and at least two insulating apertures.

7. A line conditioning electronic component as recited in claim 1, wherein said at
15 least two electrode plates have equal and balanced electrical characteristics and said at least two electrical conductors are electrically polarized opposite of one another, wherein said equal and balanced electrical characteristics in cooperation with said electrically opposite polarized at least two electrical conductors result in line-to-line capacitance values equal to approximately half of the line-to-ground capacitance values for said line
20 conditioning electronic component.

8. A line conditioning electronic component as recited in claim 1, wherein the interlacing of said at least two electrode plates and three of said at least one common

ground conductive plates creates a Faraday shield encircling and separating each of said at least two electrical conductors while reducing mutual inductive coupling between said at least two electrical conductors.

- 5 9. A line conditioning electronic component as recited in claim 1, wherein said predetermined electrical property of said material is selected from the group consisting of capacitive filtering, over voltage and surge suppression, capacitive and inductive filtering, and combinations of capacitive, inductive and suppression properties wherein the particular substance which said material is comprised of will determine the specific
- 10 performance in both filter and surge protection functions.

10. A line conditioning electronic component comprising:

at least one common ground conductive plate having a plurality of insulating apertures;

- 15 at least two electrode plates, wherein said first electrode plate is stacked below said common ground conductive plate and said second electrode plate is stacked above said common ground conductive plate, wherein said at least two electrode plates sandwich said at least one center common ground conductive plate;

said at least two electrode plates each include at least two conductive electrodes

20 each having at least one coupling aperture and at least one blocking electrode having a plurality of coupling and insulating apertures;

a plurality of electrical conductors disposed through said apertures of said at least one common ground conductive plate and said at least two electrode plates, wherein a

plurality of predetermined electrical conductors are electrically connected to each of said conductive electrodes and a plurality of predetermined electrical conductors are electrically connected to each of said blocking electrodes; and

a material having predetermined electrical properties, wherein said material is maintained between said common ground conductive plate and said at least two electrode plates preventing direct electrical connection between said plates;

wherein said combination forms a plurality of differential and common mode filters and a plurality of blocking capacitors.

10 11. A line conditioning electronic component as recited in claim 10, wherein said material having predetermined electrical properties is selected from the group consisting of dielectric materials, metal oxide varistor materials, ferrite materials, sintered polycrystalline materials and ferroelectric-ferromagnetic composite materials wherein the particular material will determine the specific performance of both filter and surge protection functions.

12. A line conditioning electronic component as recited in claim 10, further comprising at least two common ground conductive plates each having a plurality of insulating apertures, wherein said first common ground conductive plate is stacked below said first electrode plate and said second common ground conductive plate is stacked above said second electrode plate, wherein said material having predetermined electrical properties is maintained between said electrode plates and said at least two common ground conductive plates and wherein said plurality of electrical conductors are disposed

through said apertures of said first and second common ground conductive plates.

13. A line conditioning electronic component comprising:

at least one common ground conductive plate having at least two insulating

5 apertures;

at least two electrode plates, wherein each of said at least two electrode plates is comprised of a material having predetermined electrical properties, wherein each of said at least two electrode plates includes a conductive surface having a coupling aperture;

wherein each of said at least two electrode plates is coupled to opposite sides of
10 said at least one common ground conductive plate with said conductive surfaces of said electrode plates directed away from said at least one common ground conductive plate;
and

at least one pair of electrical conductors, wherein each of said electrical conductors is disposed through and connected to one of said coupling apertures of said
15 electrode plates and disposed through the respective insulating aperture of said at least one common ground conductive plate creating a capacitive element coupled between said pair of electrical conductors and creating two capacitive elements coupled between each of said electrical conductors and said common ground conductive plate.

20 14. A line conditioning electronic component as recited in claim 13, wherein said material having predetermined electrical properties is selected from the group consisting of dielectric materials, metal oxide varistor materials, ferrite materials, sintered polycrystalline materials and ferroelectric-ferromagnetic composite materials wherein the

particular material will determine the specific performance in both filter and surge protection functions.

15. A line conditioning electronic component comprising:

5 a plate having two sides with first and second apertures disposed in said plate, wherein said plate is comprised of a material having predetermined electrical properties; said first side of said plate includes a first conductive surface, wherein said first aperture is electrically coupled to said first conductive surface and said second aperture is electrically isolated from said first conductive surface;

10 said second side of said plate includes a second conductive surface, wherein said first and second apertures are electrically isolated from said second conductive surface; and

said first and second conductive surfaces are electrically isolated from each other.

15 16. A line conditioning electronic component as recited in claim 15, wherein said material having predetermined electrical properties is selected from the group consisting of dielectric materials, metal oxide varistor materials, ferrite materials, and sintered polycrystalline materials wherein the particular material will determine the specific performance of both filter and surge protection functions.

20

17. A line conditioning electronic assembly comprising:

first and second plates, each of said plates having two sides with first and second apertures disposed in said plate, wherein said first and second plates are comprised of a

material having predetermined electrical properties;

said first side of said first and second plates includes a first conductive surface, wherein said first aperture is electrically coupled to said first conductive surface and said second aperture is electrically isolated from said first conductive surface;

5 said second side of said first and second plates includes a second conductive surface, wherein said first and second apertures are electrically isolated from said second conductive surface; and

said first and second conductive surfaces of each of said first and second plates are electrically isolated from each other;

10 wherein said first and second plates are stacked with said second sides of said first and second plates adjacent and electrically coupled to one another; and

said apertures of said first and second plates align to receive a plurality of electrical conductors.

15 18. A line conditioning electronic assembly as recited in claim 17, further comprising:
a common ground conductive plate having first and second apertures disposed in said common ground conductive plate;

said common ground conductive plate is positioned between and electrically coupled to said second sides of said first and second plates; and

20 said first and second apertures of said common ground conductive plate align with said first and second apertures of said first and second plates to receive a plurality of electrical conductors.

19. A line conditioning electronic component comprising:

at least one common ground plate having a common conductive electrode and an isolation band on either end which extends the width of said at least one common ground plate;

5 at least two differential plates having a conductive electrode and an isolation band along three of said differential plates four sides, wherein said first differential plate is stacked below said common ground plate and said second differential plate is stacked above said common ground plate, wherein said first and said second differential plates are oriented so their sides which do not have isolation bands are placed in opposing directions
10 and aligned with said isolation bands of said common ground plate;

a material having predetermined electrical properties, wherein said material is maintained between said at least one common ground plate and said at least two differential plates; and

a first differential band, a second differential band and a common band, wherein
15 said conductive electrode of said first differential plate is coupled to said first differential band, wherein said conductive electrode of said second differential plate is coupled to said second differential band, and wherein said conductive electrode of said common ground plate is coupled to said common band creating a capacitive element coupled between said first and second differential bands and two capacitive elements coupled between each of
20 said first and second differential bands and said common band.

20. A line conditioning electronic component as recited in claim 19, wherein said material having predetermined electrical properties is selected from the group consisting

of dielectric materials, metal oxide varistor materials, ferrite materials, sintered polycrystalline materials and ferroelectric-ferromagnetic composite materials wherein the particular material will determine the specific performance in both filter and surge protection functions.

5

21. A line conditioning electronic component as recited in claim 19, further comprising a plurality of differential plates and a plurality of common ground plates, wherein each of said plurality of differential plates and each of said common ground plates cooperates to form a capacitive element coupled between each pair of said differential bands and creating a capacitive element coupled between each of said differential bands and said common band.

10

22. A line conditioning electronic component as recited in claim 19, wherein said at least two electrode plates have equal and balanced electrical characteristics and said at least two electrical conductors are electrically polarized opposite of one another, wherein said equal and balanced electrical characteristics in cooperation with said electrically opposite polarized at least two electrical conductors result in line-to-line capacitance values equal to approximately half of the line-to-ground capacitance values for said line conditioning electronic component.

15

20

23. A line conditioning electronic component as recited in claim 19, wherein the interlacing of said at least two differential plates and said at least one common ground plate creates a Faraday shield encircling and separating each of said first and second

differential bands while reducing mutual inductive coupling between said first and second differential bands.

24. A line conditioning electronic component as recited in claim 19, wherein said
5 predetermined electrical property of said material is selected from the group consisting of capacitive filtering, over voltage and surge suppression, capacitive and inductive filtering, and combinations of capacitive, inductive and suppression properties wherein the particular substance which said material is comprised of will determine the specific performance in both filter and surge protection functions.

10

25. A line conditioning electronic component comprising:

at least one common ground plate having a common conductive electrode and an isolation band on either end which extends the width of said at least one common ground plate;

15

at least two differential plates having a conductive electrode and an isolation band along three of said differential plates four sides, wherein said first differential plate is stacked below said common ground plate and said second differential plate is stacked above said common ground plate, wherein said first and said second differential plates are oriented so their sides which do not have isolation bands are placed in opposing directions
20 and aligned with said isolation bands of said common ground plate;

a material having predetermined electrical properties, wherein said material is maintained between said at least one common ground plate and said at least two differential plates; and

a first differential band, a second differential band and a common band, wherein said conductive electrode of said first differential plate is coupled to said first differential band, wherein said conductive electrode of said second differential plate is coupled to said second differential band, and wherein said conductive electrode of said common ground plate is coupled to said common band creating a capacitive element coupled between said first and second differential bands and two capacitive elements coupled between each of said first and second differential bands and said common band.

26. A line conditioning electronic assembly comprising at least two line conditioning electronic components as recited in claim 25, wherein said first and second line conditioning electronic components are stacked upon each other; and

said first differential bands of said first and second line conditioning electronic components are electrically coupled to one another, said second differential bands of said first and second line conditioning electronic components are electrically coupled to one another, and said common bands of said first and second line conditioning electronic components are electrically coupled to one another, thereby electrically coupling said first and second line conditioning electronic components in parallel.

26. A line conditioning electronic assembly as recited in claim 26, further comprising at least two additional common ground plates wherein said first additional common ground plate is stacked above said line conditioning electronic assembly and said second additional common ground plate is stacked below said line conditioning electronic assembly.

27. A line conditioning electronic assembly as recited in claim 26, further comprising an additional common ground plate between said at least two line conditioning electronic components thereby providing increased electrical isolation between said first and second line conditioning electronic components.

5

28. A line conditioning electronic assembly comprising a line conditioning electronic component as recited in claim 25, wherein said line conditioning electronic component and a capacitor are stacked upon each other, and

said capacitor is electrically coupled between said first and said second differential

10 bands of said line conditioning electronic component.

29. A line conditioning electronic component comprising:

at least one common ground conductive plate formed upon a support material having predetermined electrical properties;

15 a plurality of first and second electrode plates, wherein said plurality of first electrode plates are formed upon a first support material having predetermined electrical properties and said plurality of second electrode plates are formed upon a second support material having predetermined electrical properties;

wherein said plurality of first electrode plates are stacked above said at least one
20 common ground conductive plate and said plurality of second electrode plates are stacked below said at least one common ground conductive plate, wherein said plurality of said first electrode plates and said plurality of said second electrode plates sandwich said at least one center common ground conductive plate;

wherein said support material isolates said common ground conductive plate, said plurality of first electrode plates and said plurality of second electrode plates preventing direct electrical connection between said plates; and

said at least one common ground conductive plate, said plurality of first electrode
5 plates, said plurality of second electrode plates and said support material form a plurality of differential and common mode filters.

30. A line conditioning electronic component as recited in claim 29, wherein said support material having predetermined electrical properties is selected from the group
10 consisting of dielectric materials, metal oxide varistor materials, ferrite materials, sintered polycrystalline materials and ferroelectric-ferromagnetic composite materials wherein the particular material will determine the specific performance of both filter and surge protection functions.

15 31. A line conditioning electronic component as recited in claim 29, further comprising a material having predetermined electrical properties, wherein said material is maintained between said at least one common ground conductive plate and said plurality of first and second electrode plates preventing direct electrical connection between said plates.

20

32. A line conditioning electronic component as recited in claim 29, further comprising a plurality of first differential bands, a plurality of second differential bands and a plurality of common bands;

wherein each of said plurality of first electrode plates is electrically connected to one of said plurality of first differential bands;

wherein each of said plurality of second electrode plates is electrically connected to one of said plurality of second differential bands; and

5 wherein said at least one common ground conductive plate is electrically connected to each of said plurality of common bands, thereby forming a capacitive element between each of said first and second differential bands and two capacitive elements between each of said first and second differential bands and said plurality of common bands.

10

33. A line conditioning electronic component as recited in claim 29, further comprising at least two common ground conductive plates, wherein said first common ground conductive plate is stacked above said plurality of said first electrode plates and said second common ground conductive plate is stacked below said plurality of said
15 second electrode plates.

34. A line conditioning electronic component comprising:

at least one common ground conductive plate formed upon a support material having predetermined electrical properties;

20 first and second electrode plates, wherein said first electrode plate is formed upon a first support material having predetermined electrical properties and said second electrode plate is formed upon a second support material having predetermined electrical properties;

wherein said first electrode plate is stacked above said at least one common ground conductive plate and said second electrode plate is stacked below said at least one common ground conductive plate, wherein said first electrode plate and said second electrode plate sandwich said at least one center common ground conductive plate;

5 wherein said support material isolates said common ground conductive plate, said first electrode plate and said second electrode plate preventing direct electrical connection between said plates; and

 said at least one common ground conductive plate, said first electrode plate, said second electrode plate and said support material form a plurality of differential and
10 common mode filters.

35. A line conditioning electronic component as recited in claim 34, wherein said support material having predetermined electrical properties is selected from the group consisting of dielectric materials, metal oxide varistor materials, ferrite materials, sintered
15 polycrystalline materials and ferroelectric-ferromagnetic composite materials wherein the particular material will determine the specific performance of both filter and surge protection functions.

36. A line conditioning electronic component as recited in claim 34, further
20 comprising a plurality of first differential bands, a plurality of second differential bands and at least one common band;

 wherein said first electrode plate is electrically connected to one of said plurality of first differential bands;

wherein said second electrode plate is electrically connected to one of said plurality of second differential bands; and

wherein said at least one common ground conductive plate is electrically connected to said at least one common band, thereby forming a capacitive element between said first and second differential bands and two capacitive elements between each of said first and second differential bands and said at least one common band.

37. A line conditioning electronic component as recited in claim 34, further comprising at least two common ground conductive plates, wherein said first common ground conductive plate is stacked above said first electrode plate and said second common ground conductive plate is stacked below said second electrode plate.

38. A line conditioning electronic assembly comprised of at least a first and second line conditioning electronic component as recited in claim 37, wherein said first and second line conditioning electronic components are stacked upon each other, thereby electrically coupling said first and second line conditioning electronic components in parallel.

39. A line conditioning electronic component comprising:
at least one common conductive plate having an isolation barrier on either end which extends the width of said at least one common conductive plate, wherein said common conductive plate comprises a film having a conductive surface deposited upon said film, and wherein said isolation barriers are formed by removing predetermined

portions of said conductive surface;

at least two electrode plates each having a first isolation barrier and a second isolation barrier, wherein said first isolation barrier and said second isolation barrier divide each of said electrode plates into three electrically isolated areas with the area
5 within said first isolation barrier forming the primary electrode pattern;

said first electrode plate is stacked below said common conductive plate and said second electrode plate is stacked above said common conductive plate, wherein said first and said second electrode plates are aligned so their first isolation barriers are positioned opposite one another, and wherein said at least two electrode plates sandwich said at least
10 one common conductive plate; and

at least two conductive terminal, wherein said first terminal is coupled to said primary electrode pattern of said first electrode plate and said second terminal is coupled to said primary electrode pattern of said second electrode plate creating a capacitive element coupled between said first and said second terminals and creating two capacitive
15 elements coupled between each of said first and said second terminals and said common conductive plate.

40. A line conditioning electronic component as recited in claim 39, wherein said at least two electrode plates have equal and balanced electrical characteristics and said at
20 least two conductive terminals are electrically polarized opposite of one another, wherein said equal and balanced electrical characteristics in cooperation with said electrically opposite polarized at least two electrical conductors result in line-to-line capacitance values equal to approximately half of the line-to-ground capacitance values for said line

conditioning electronic component.

41. A line conditioning electronic component as recited in claim 39, wherein the interlacing of said at least two electrode plates and said at least one common conductive
5 plate creates a Faraday shield encircling each of said at least two electrical conductors while reducing mutual inductive coupling between said at least two electrical conductors.

42. A line conditioning electronic component as recited in claim 39, wherein said predetermined electrical property of said conductive surface of said film is selected from
10 the group consisting of capacitive filtering, over voltage and surge suppression, capacitive and inductive filtering, and combinations of capacitive, inductive and suppression properties wherein the particular substance which said material is comprised of will determine the specific performance in both filter and surge protection functions.

15 43. A motor line conditioning electronic component comprising:
at least one common conductive electrode;
at least two conductive electrodes, wherein said first conductive electrode is stacked below said common conductive electrode and said second conductive electrode is stacked above said common conductive electrode, wherein said at least two conductive
20 electrodes sandwich said at least one common conductive electrode;
a material having predetermined electrical properties, wherein said material is maintained between said at least one common conductive electrode and said at least two conductive electrodes; and

a first conductive band, a second conductive band and a common band, wherein said first conductive band is coupled to said first conductive electrode and said second conductive band is coupled to said second conductive electrode, and wherein said common conductive electrode is coupled to said common band creating a capacitive element coupled between said first and said second conductive bands and two capacitive elements coupled between each of said first and said second conductive bands and said common band.

44. A motor line conditioning electronic component as recited in claim 43, wherein said material having predetermined electrical properties is selected from the group consisting of dielectric materials, metal oxide varistor materials, ferrite materials, and sintered polycrystalline materials wherein the particular material will determine the specific performance in both filter and surge protection functions.

45. A line conditioning electronic component comprising:
at least one common conductive plate;
at least two plates of material having predetermined electrical properties; and
at least two conductive electrode plates wherein said first conductive electrode plate is stacked below said common conductive plate and said second conductive electrode plate is stacked above said common conductive plate, wherein said plates of material having predetermined electrical properties are maintained between and physically separate said common conductive plate from said first and said second conductive electrode plates.

46. A line conditioning electronic component comprising:

at least one common ground conductive plate having at least two insulating apertures;

at least two electrode plates each having at least one insulating aperture and at least one coupling aperture, wherein said first electrode plate is stacked below said common ground conductive plate and said second electrode plate is stacked above said common ground conductive plate, wherein said at least two electrode plates sandwich said at least one center common ground conductive plate;

at least two electrical conductors disposed through said apertures of said common ground conductive plate and said at least two electrode plates, wherein each of said at least two conductors is electrically connected to a different electrode plate; and

a material having predetermined electrical properties, wherein said material is maintained between said common ground conductive plate and said at least two electrode plates preventing direct electrical connection between said plates creating a capacitive element coupled between said at least two electrical conductors and creating two capacitive elements, one coupled between one electrical conductor and said common ground conductive plate and the other coupled between the other electrical conductor and said common ground conductive plate.

47. A line conditioning electronic assembly comprising a line conditioning electronic component as recited in claim 46 and a first MOV component, wherein said first MOV component is stacked on said line conditioning electronic component and said first MOV component is electrically coupled between said first electrode plate and said common

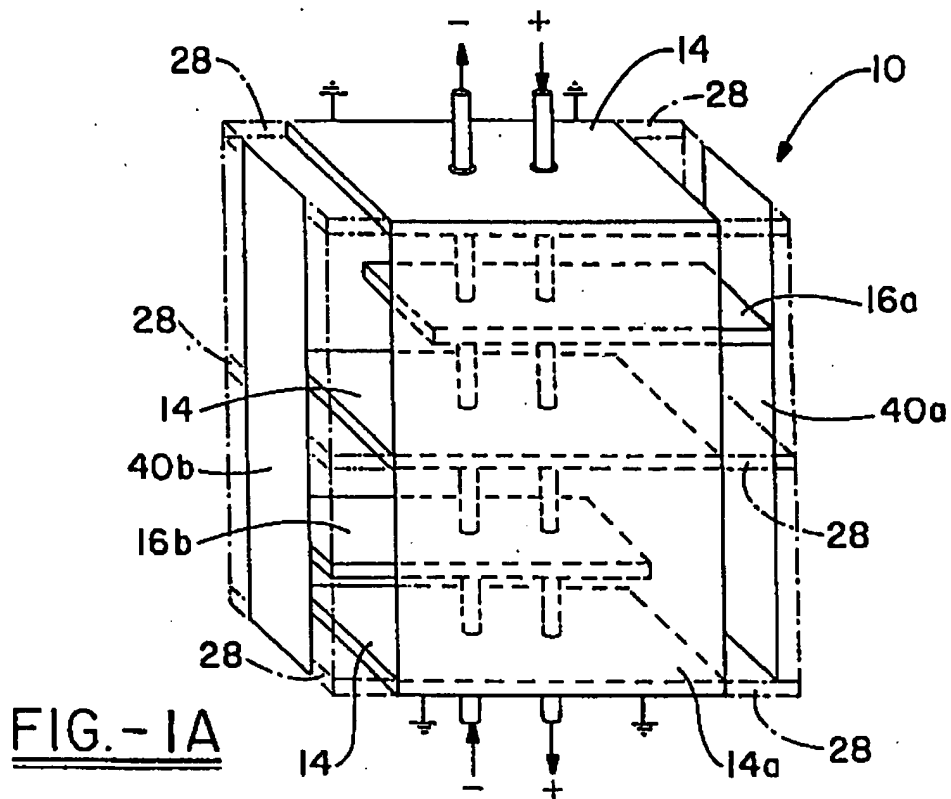
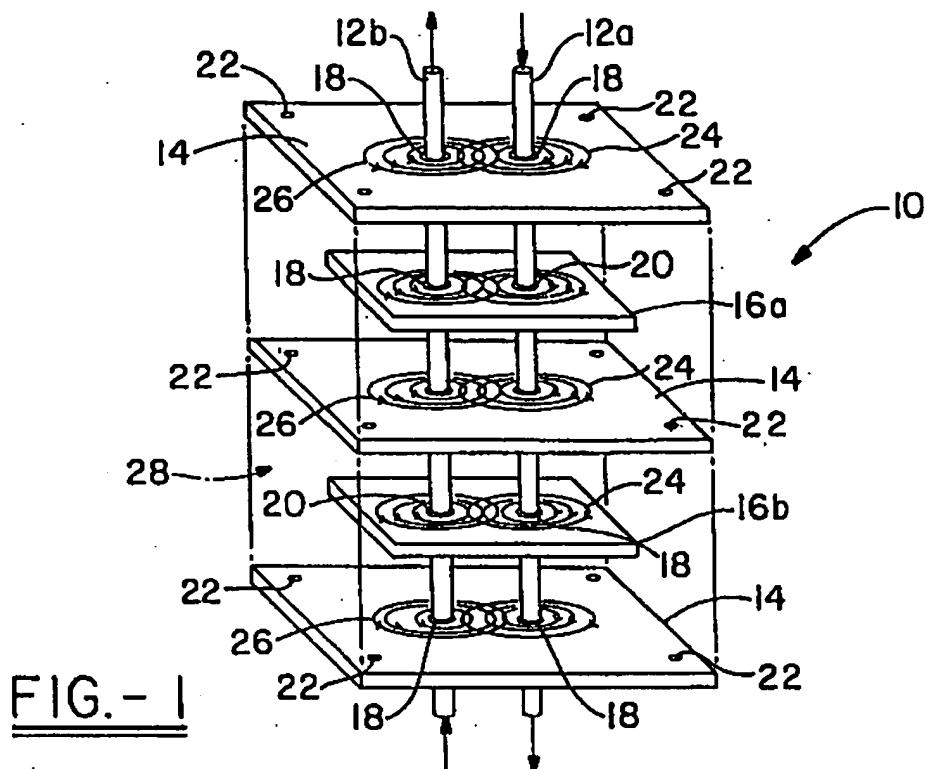
ground conductive plate.

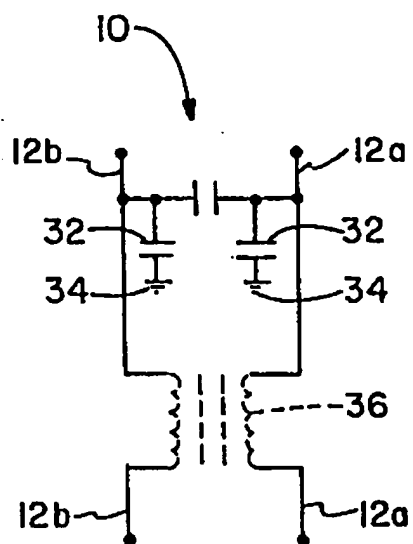
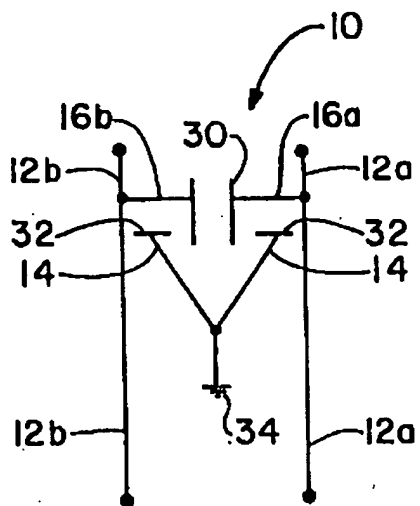
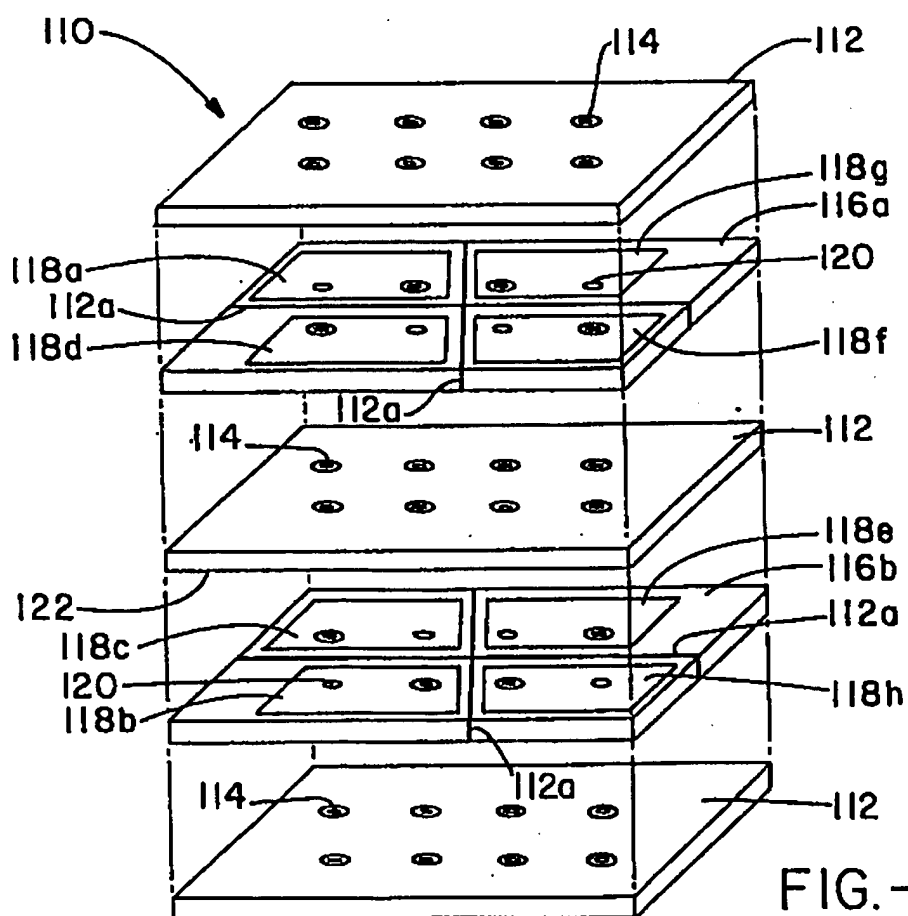
48. A line conditioning electronic assembly as recited in claim 47 further comprising a second MOV component, wherein said second MOV component is stacked on said line conditioning electronic component and said second MOV component is electrically
5 coupled between said second electrode plate and said common ground conductive plate.

49. A line conditioning electronic assembly as recited in claim 25, further comprising:
first and second inductive enclosures wherein said first inductive enclosure is
10 coupled to said first differential band and said second inductive enclosure is coupled to said second differential band;
at least one conductive terminal coupled to said common band; and
a plurality of terminals, wherein at least one of said plurality of terminals is
coupled to said first inductive enclosure and at least one of said plurality of terminals is
15 coupled to said second inductive enclosure.

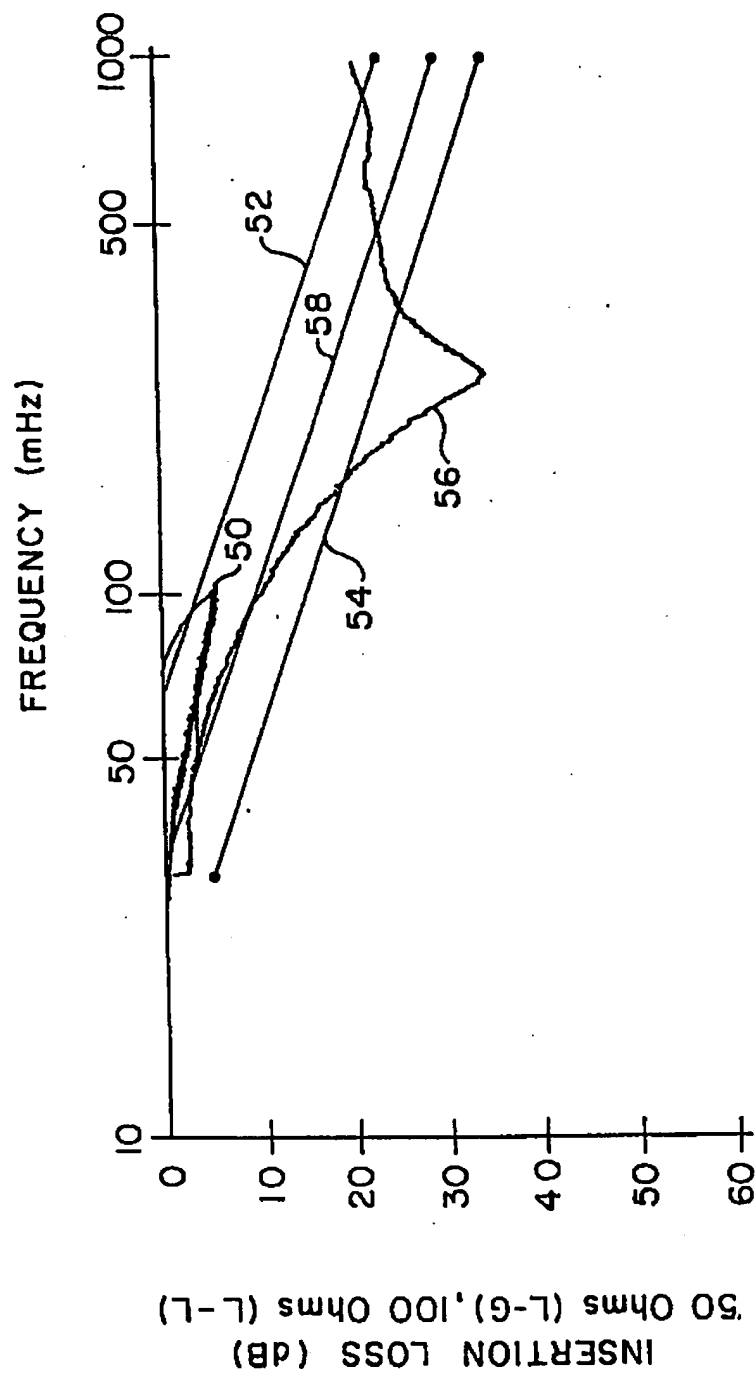
50. A line conditioning electronic assembly as recited in claim 49, wherein said enclosures each include at least one aperture in which at least one of said plurality of terminals is disposed thereby making electrical contact with said corresponding
20 differential band.

51. A line conditioning electronic assembly as recited in claim 49, wherein said first and second inductive enclosures are comprised of a ferrite material.



FIG. - 2AFIG. - 2BFIG. - 4

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FIG.-3

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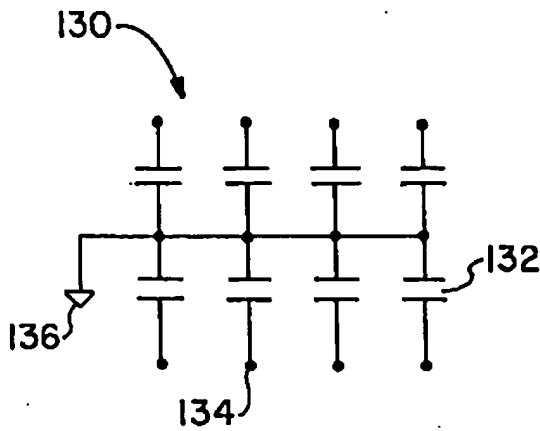


FIG. -5A

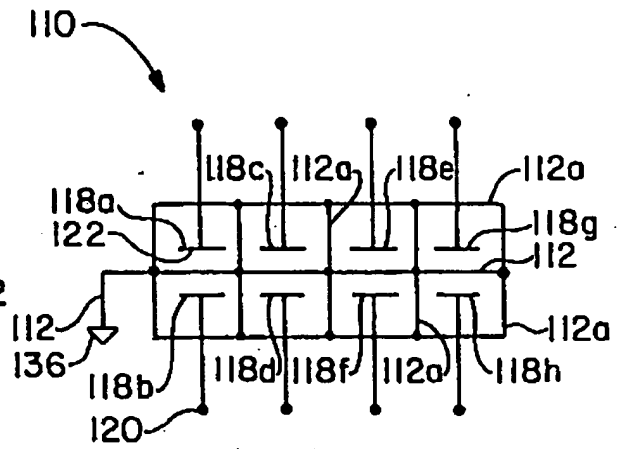


FIG. -5B

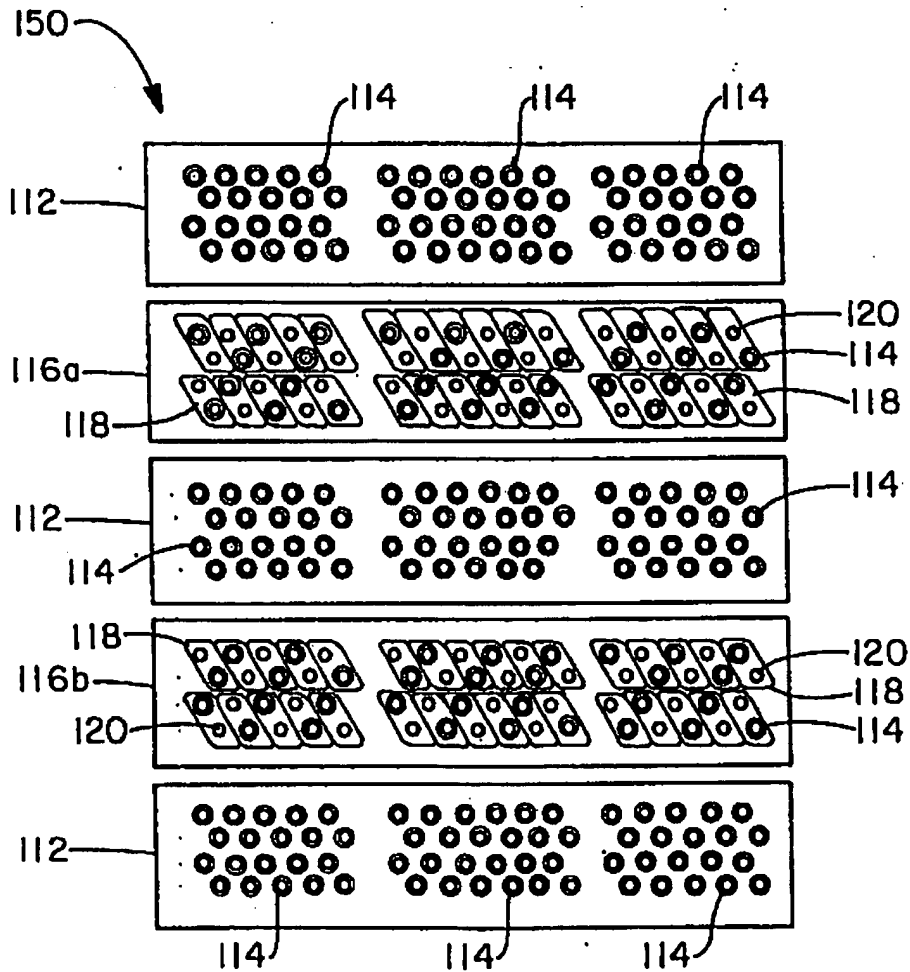
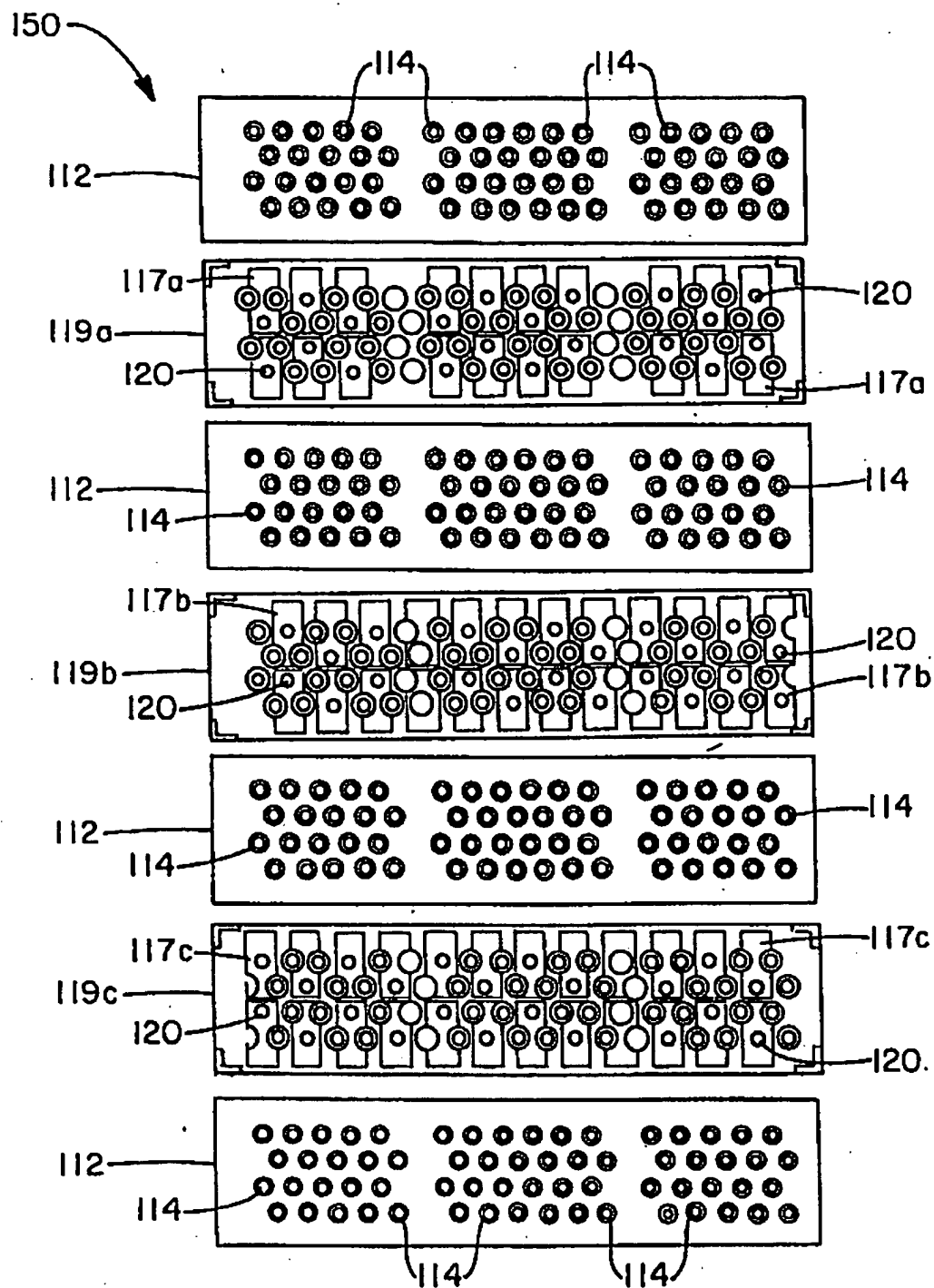


FIG. -6

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FIG.-6A

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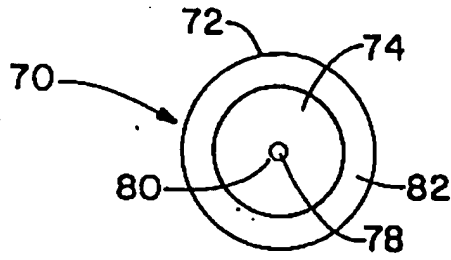


FIG. - 7A

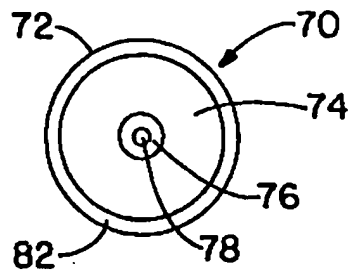


FIG. - 7B

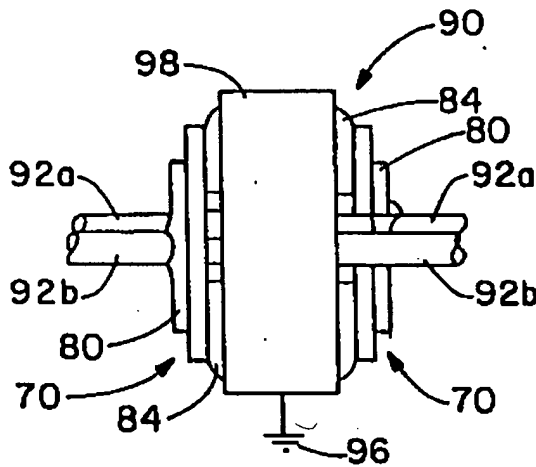


FIG. - 8

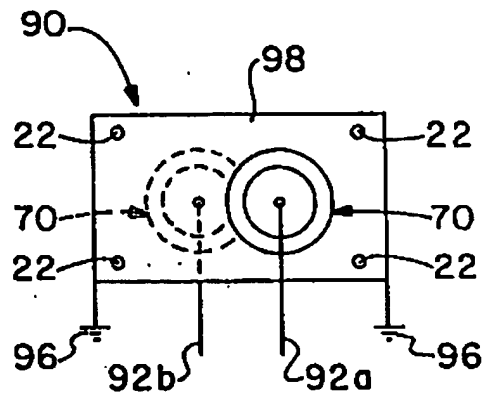


FIG. - 9

FIG. - 10A

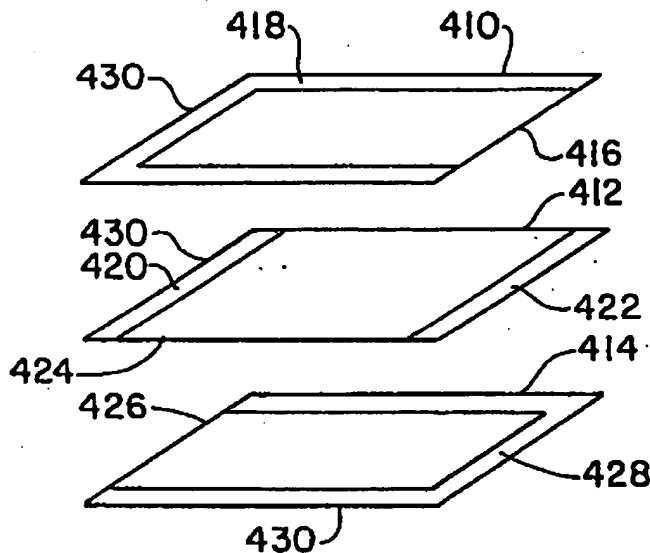
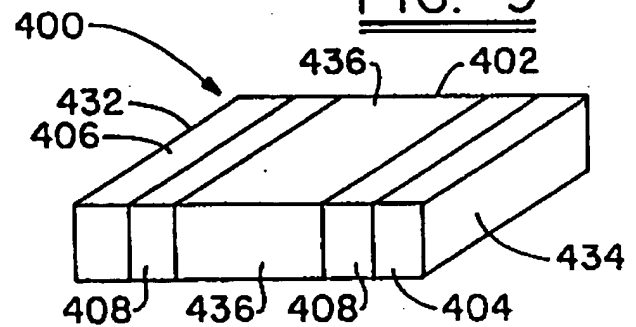
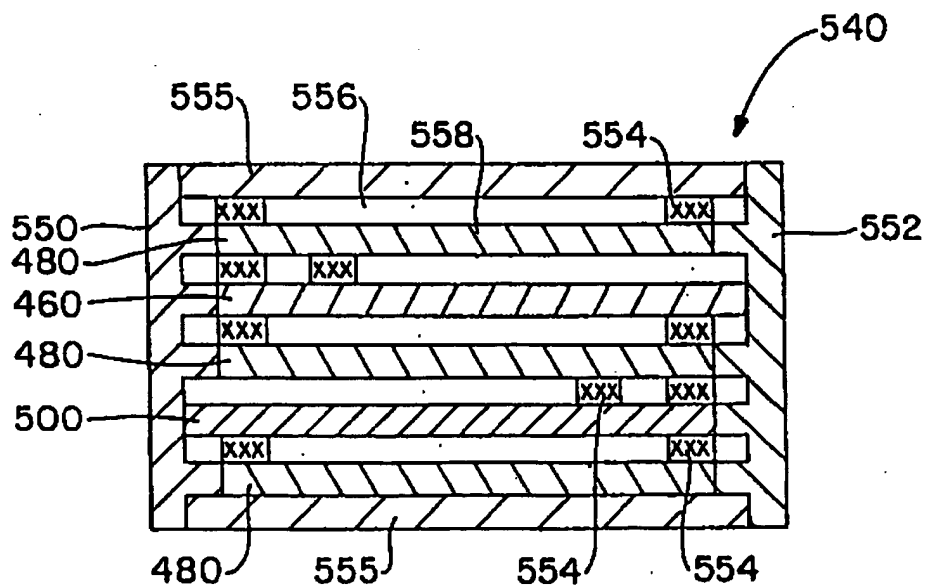
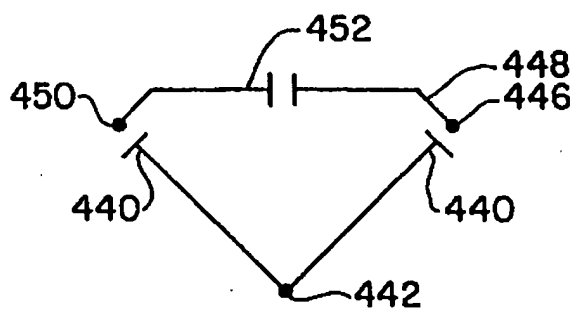
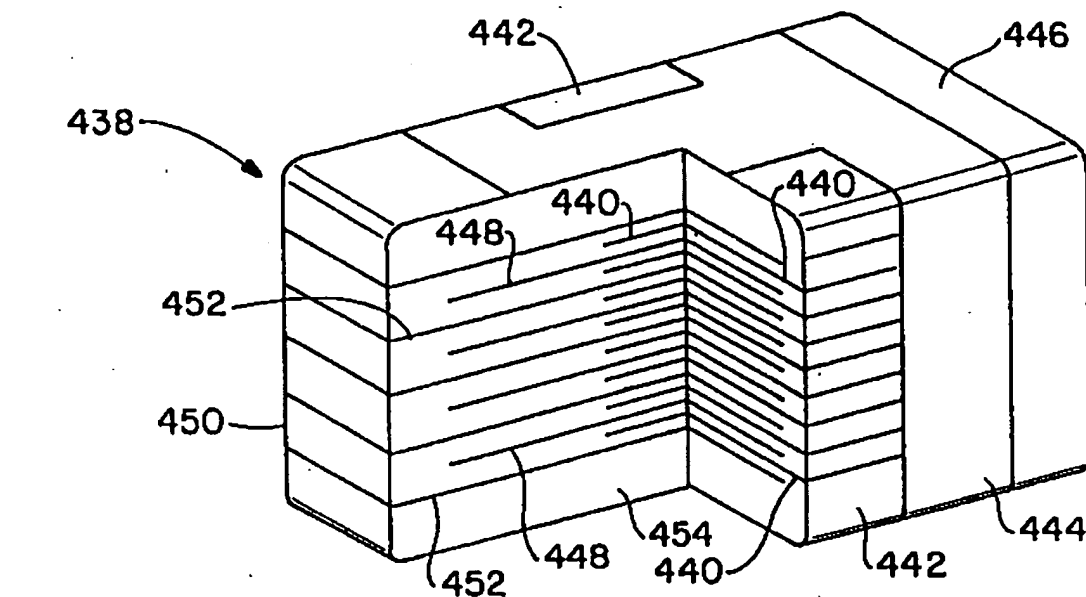


FIG. - 10B

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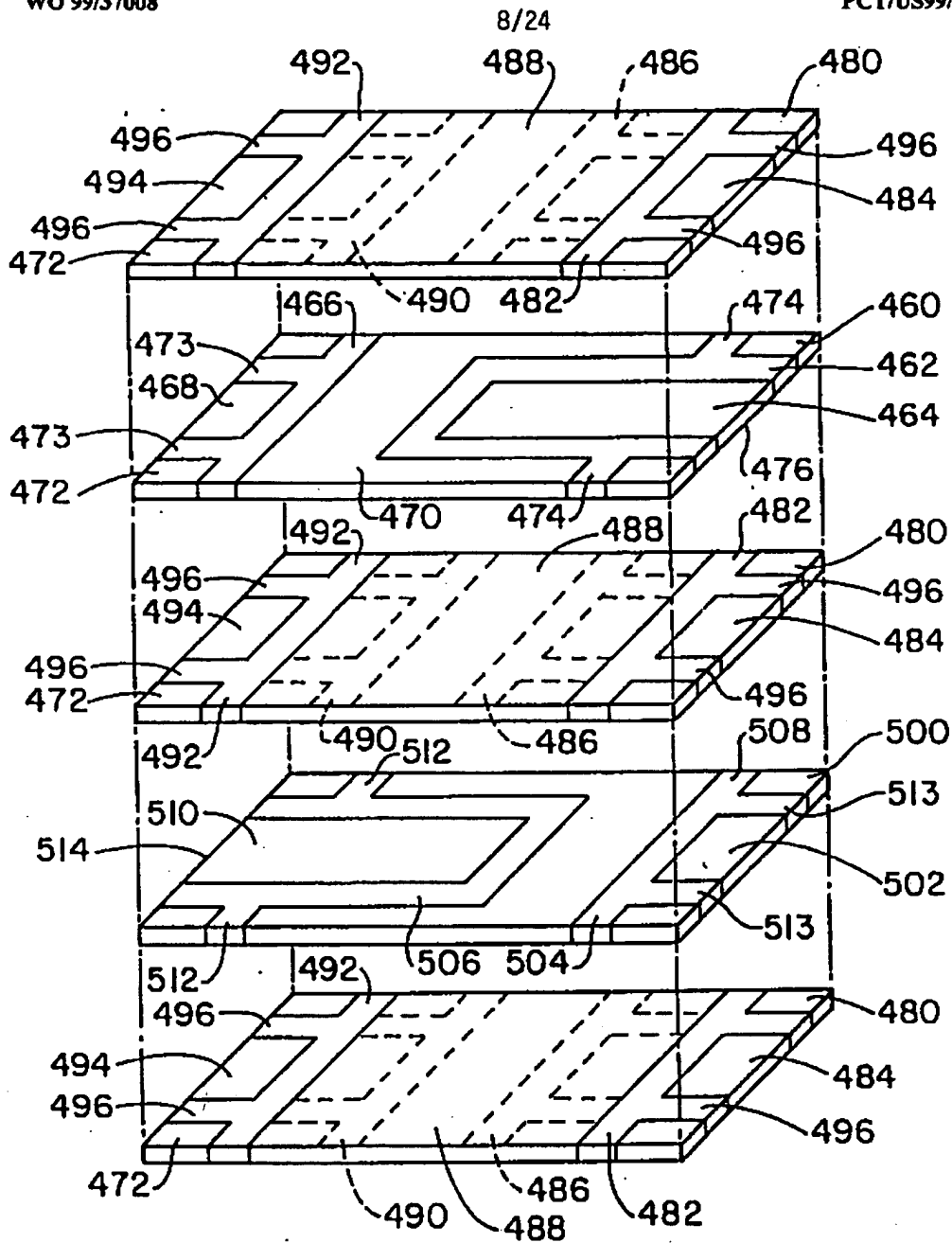
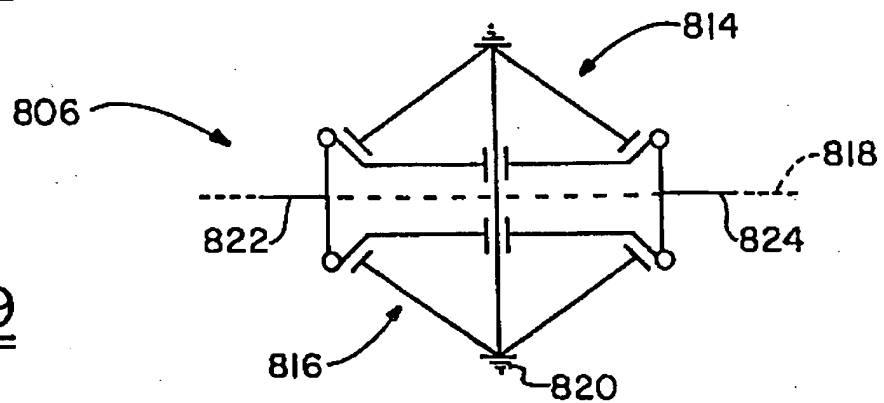


FIG.-14

FIG.-39



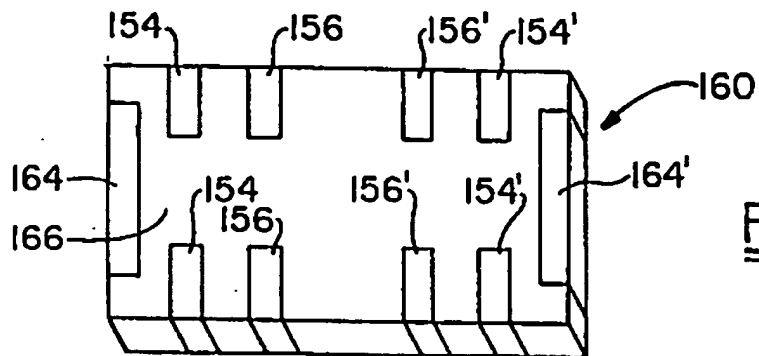


FIG. - 12A

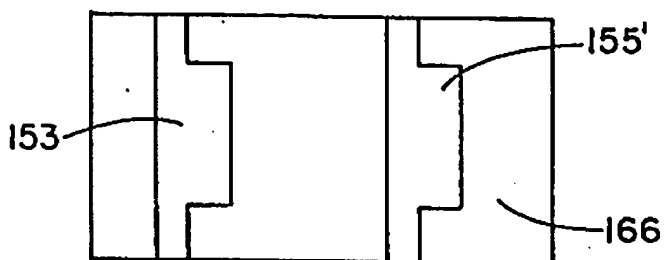


FIG. - 12B

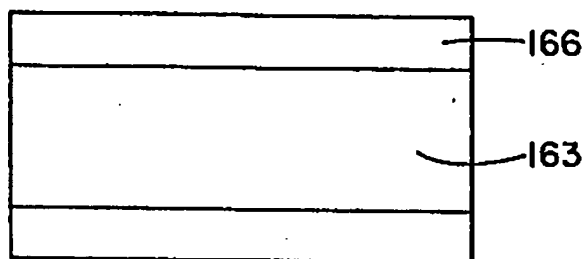


FIG. - 12C

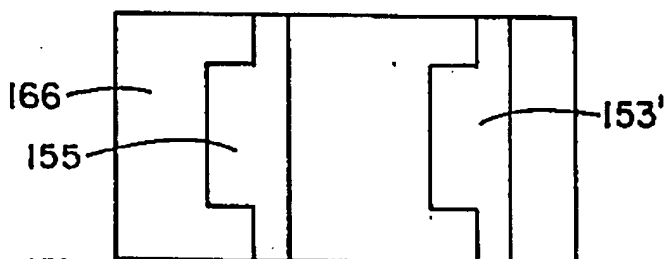


FIG. - 12D

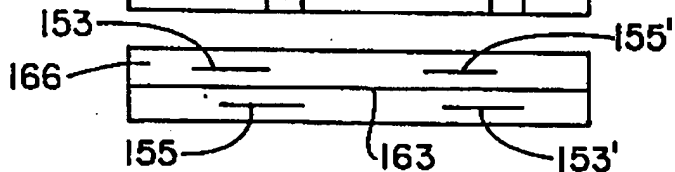


FIG. - 12E

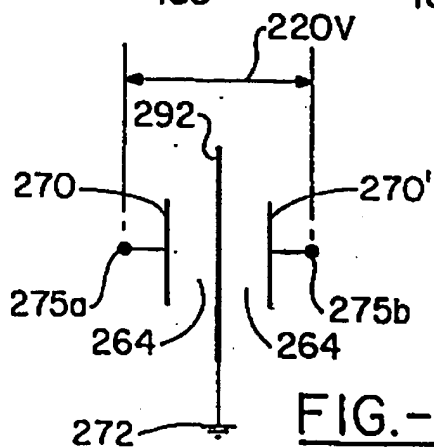


FIG. - 20A

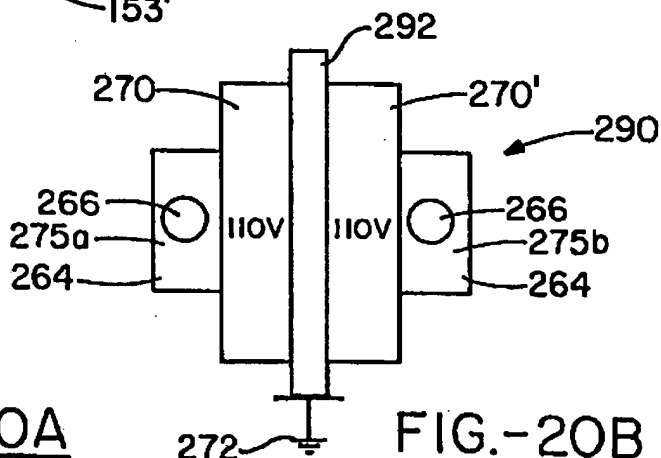


FIG. - 20B

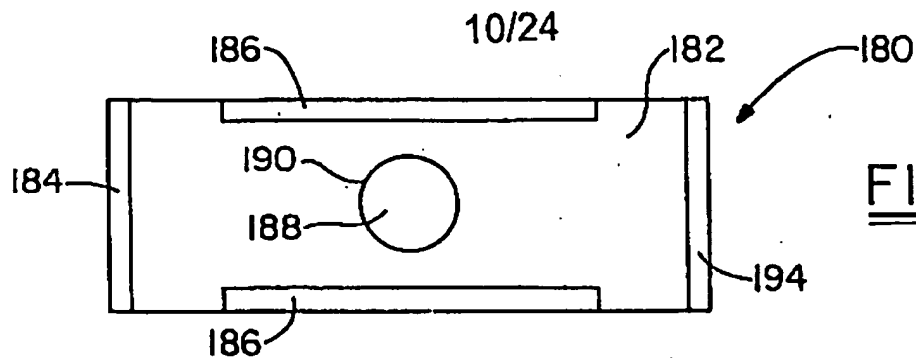


FIG.-16A



FIG.-16B

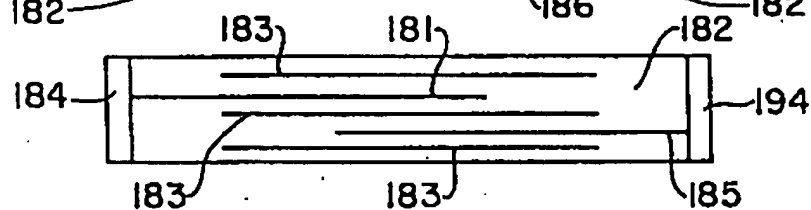


FIG.-16C

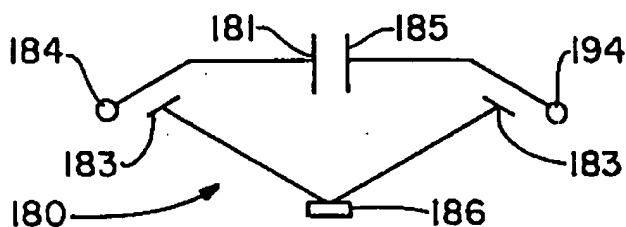


FIG.-16D

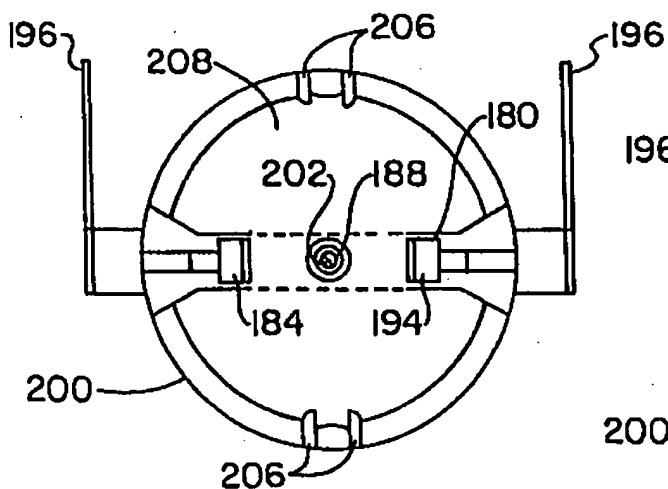


FIG.-17A

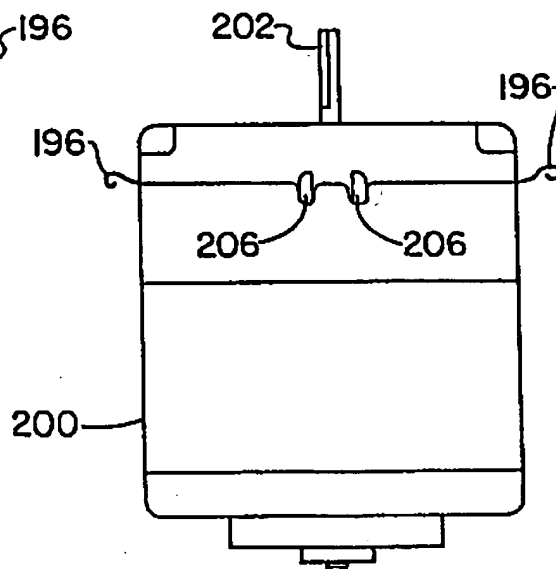
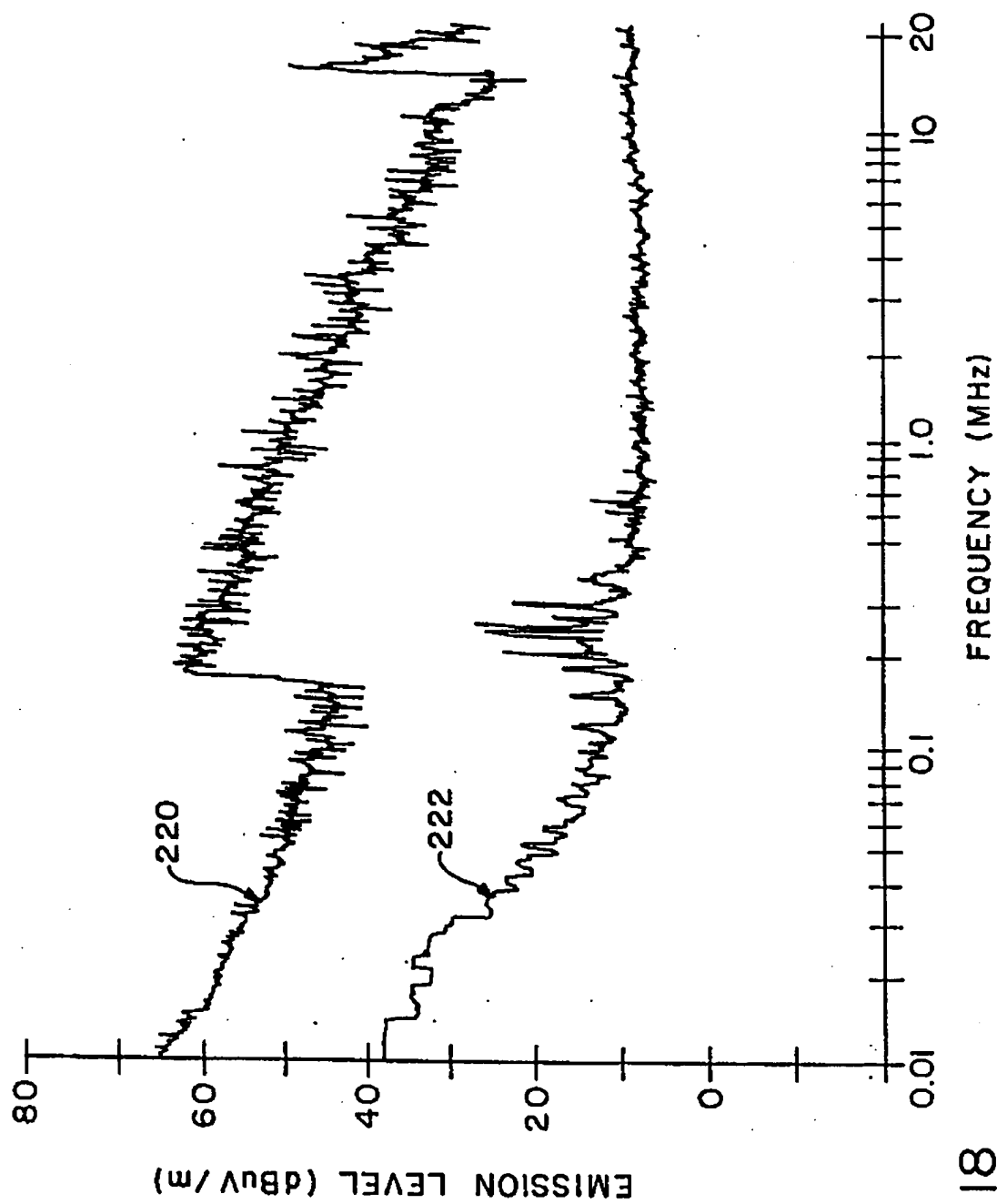


FIG.-17B

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FIG.-18

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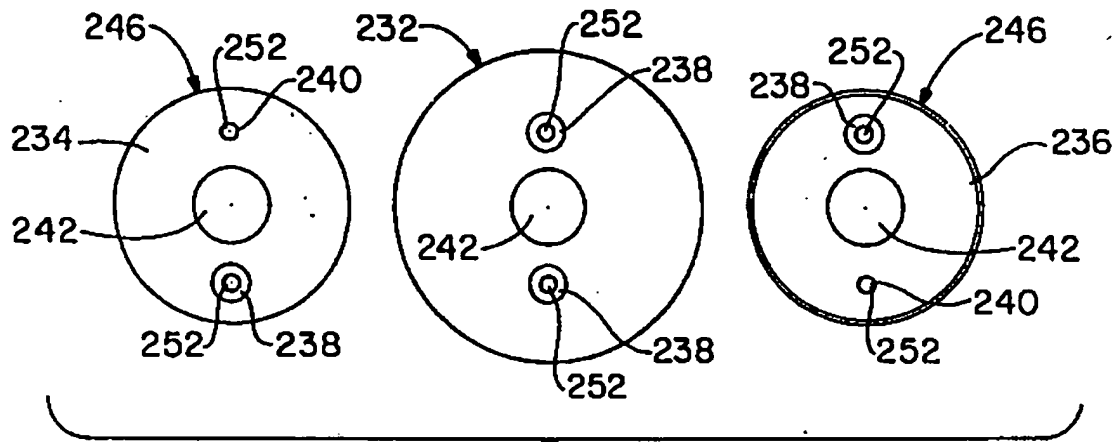


FIG. -19A

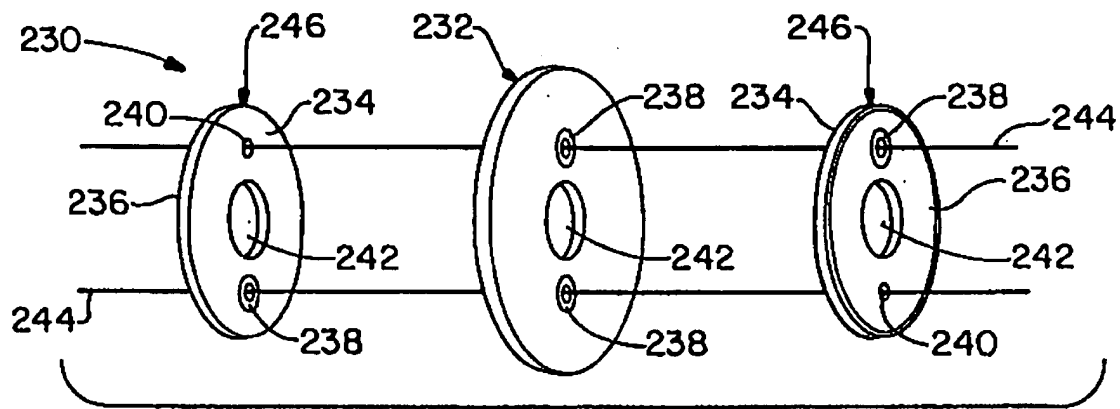


FIG. -19B

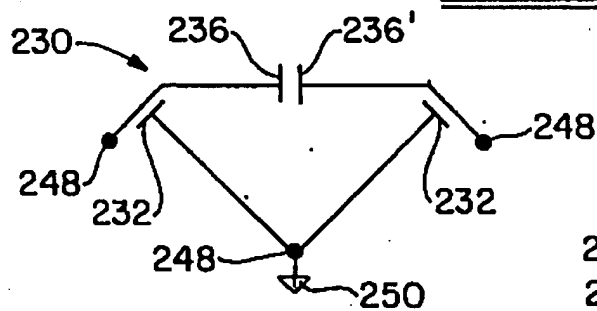


FIG. -19C

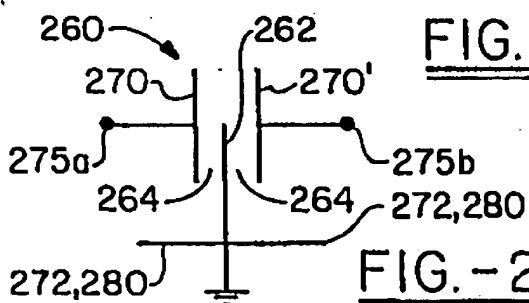
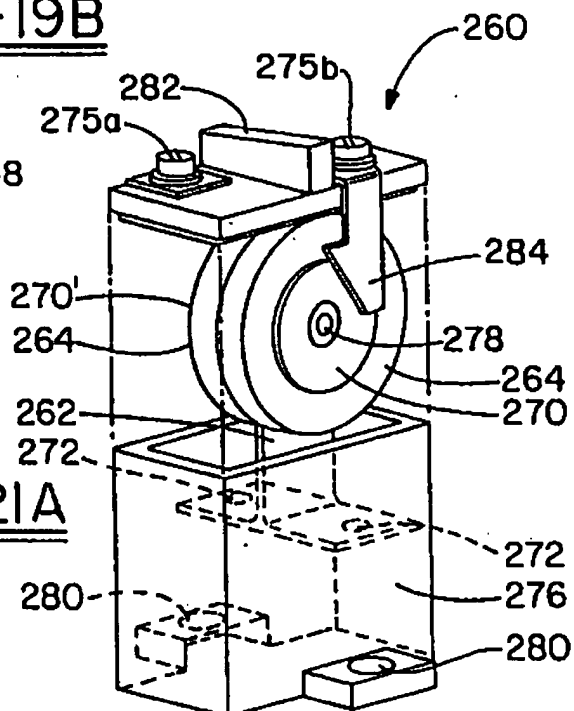


FIG. -21B



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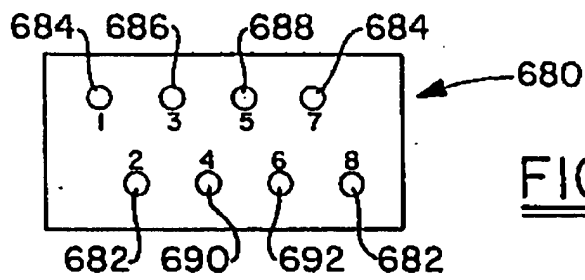
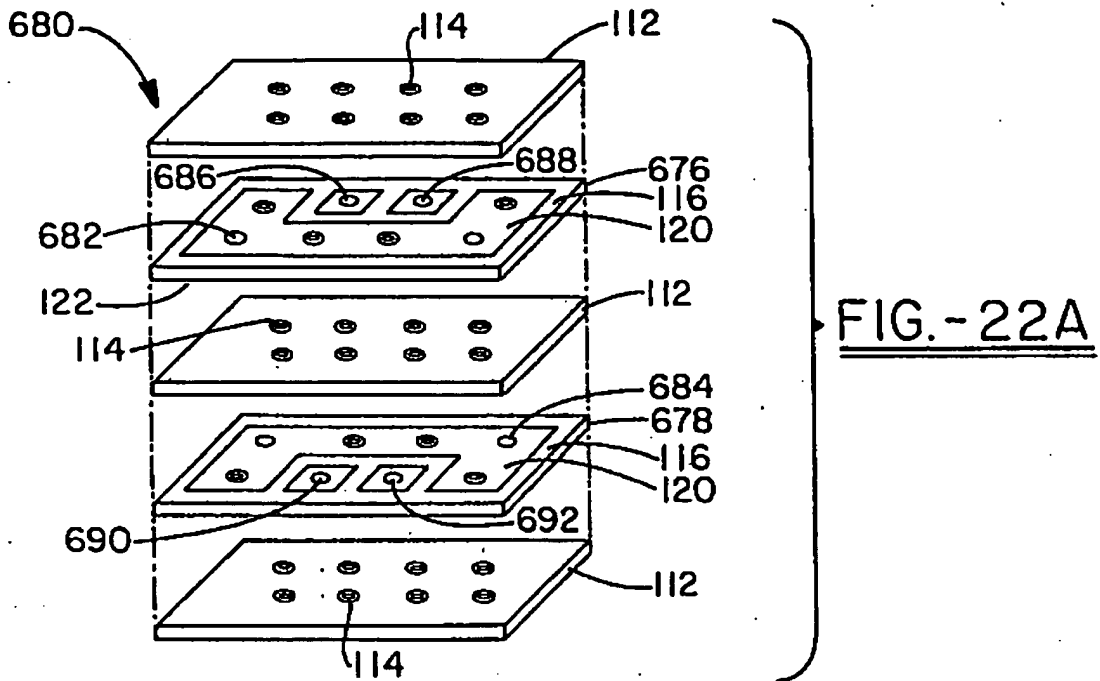


FIG.-22C.

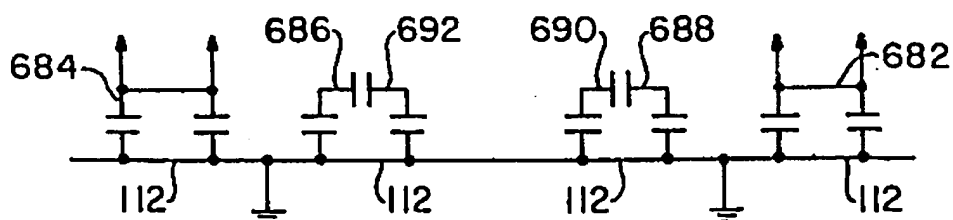
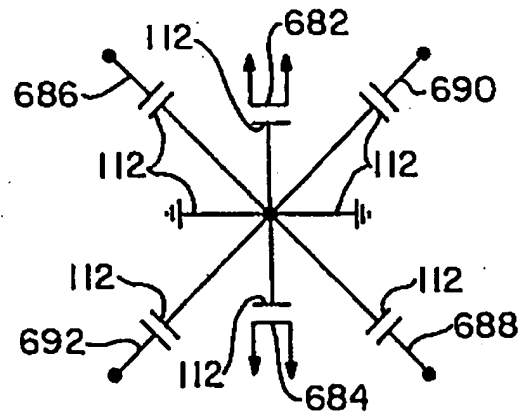


FIG.-22D

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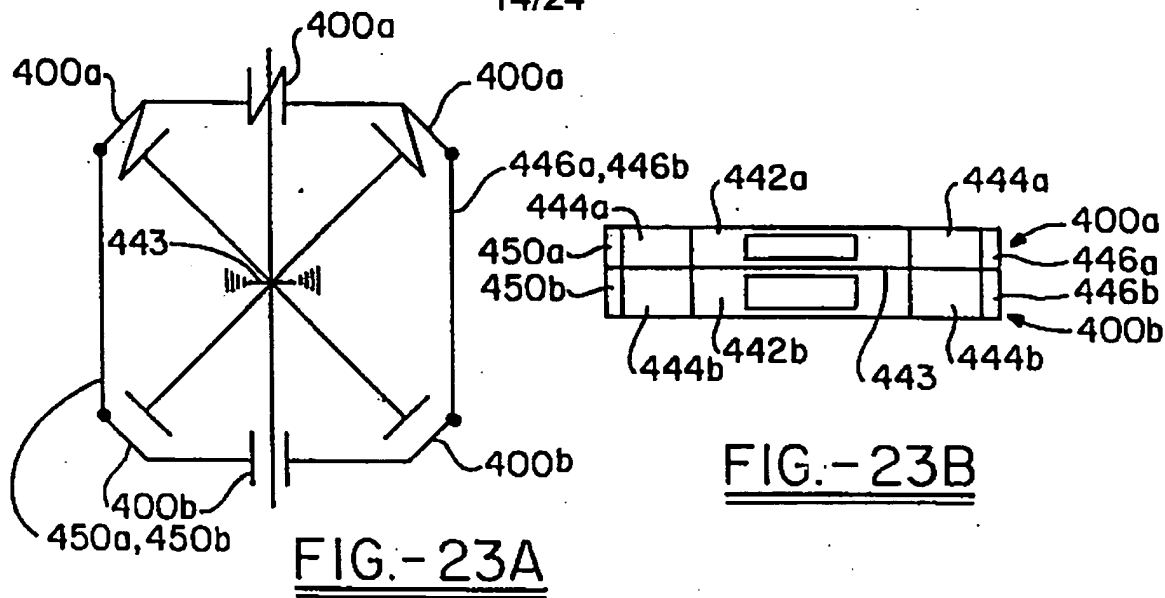


FIG.-23B

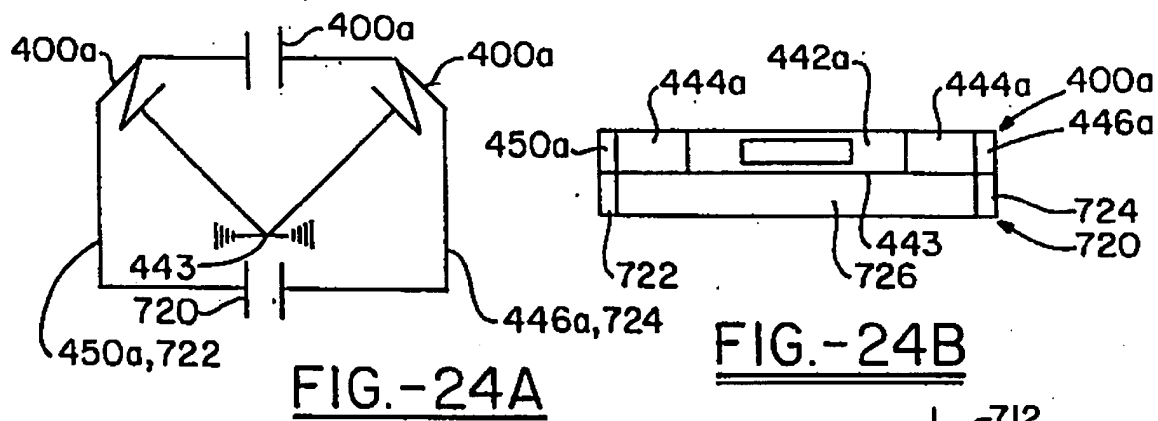


FIG.-24B

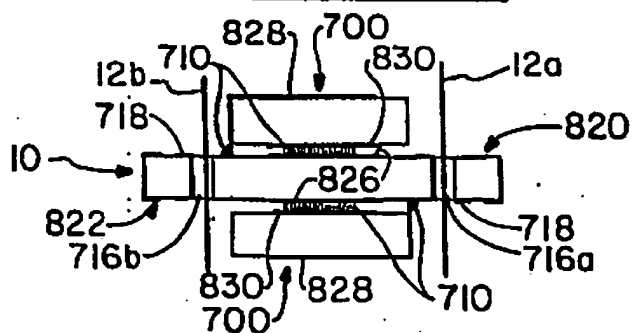


FIG.-25A

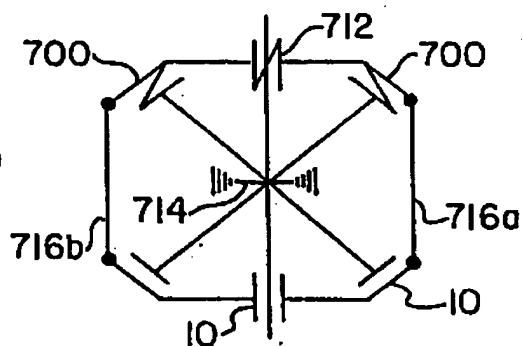
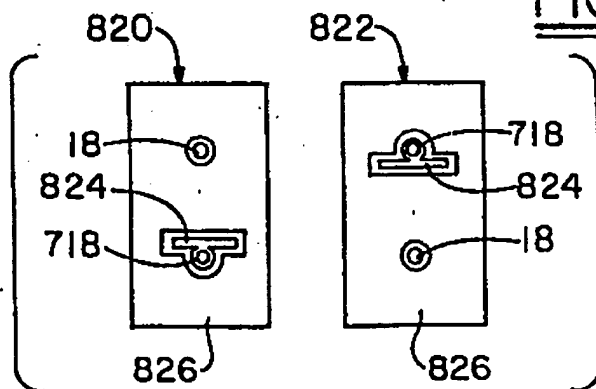


FIG.-25B

FIG.-25C



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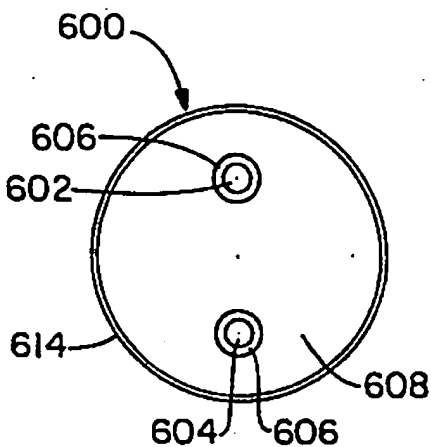


FIG. - 26A

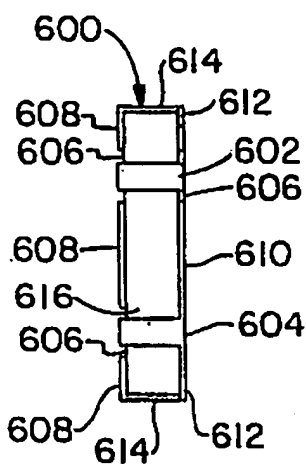


FIG. - 26B

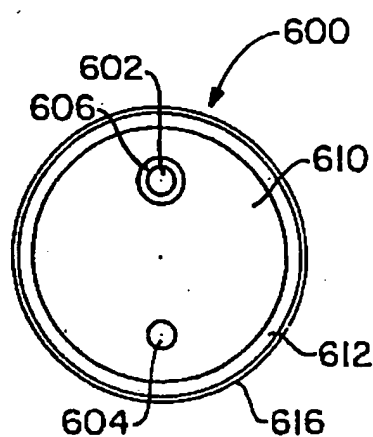


FIG. - 26C

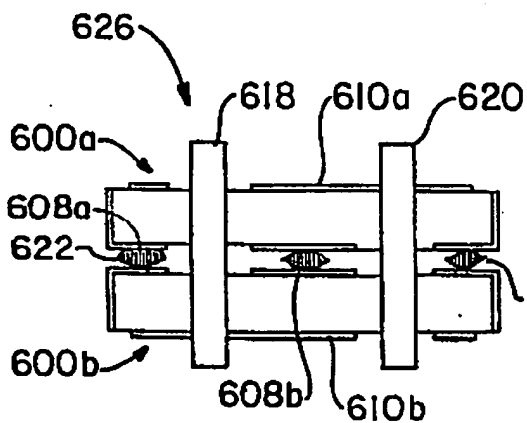


FIG. - 27

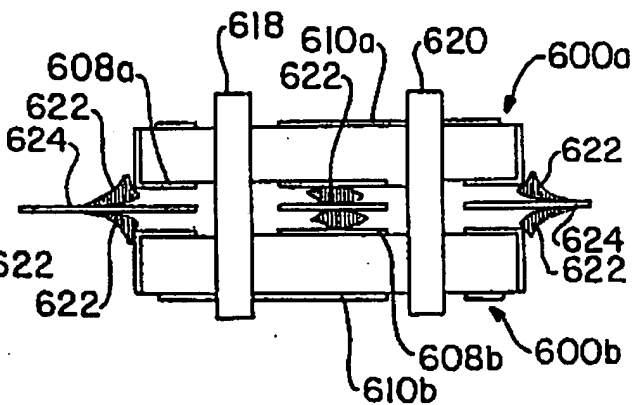


FIG. - 28

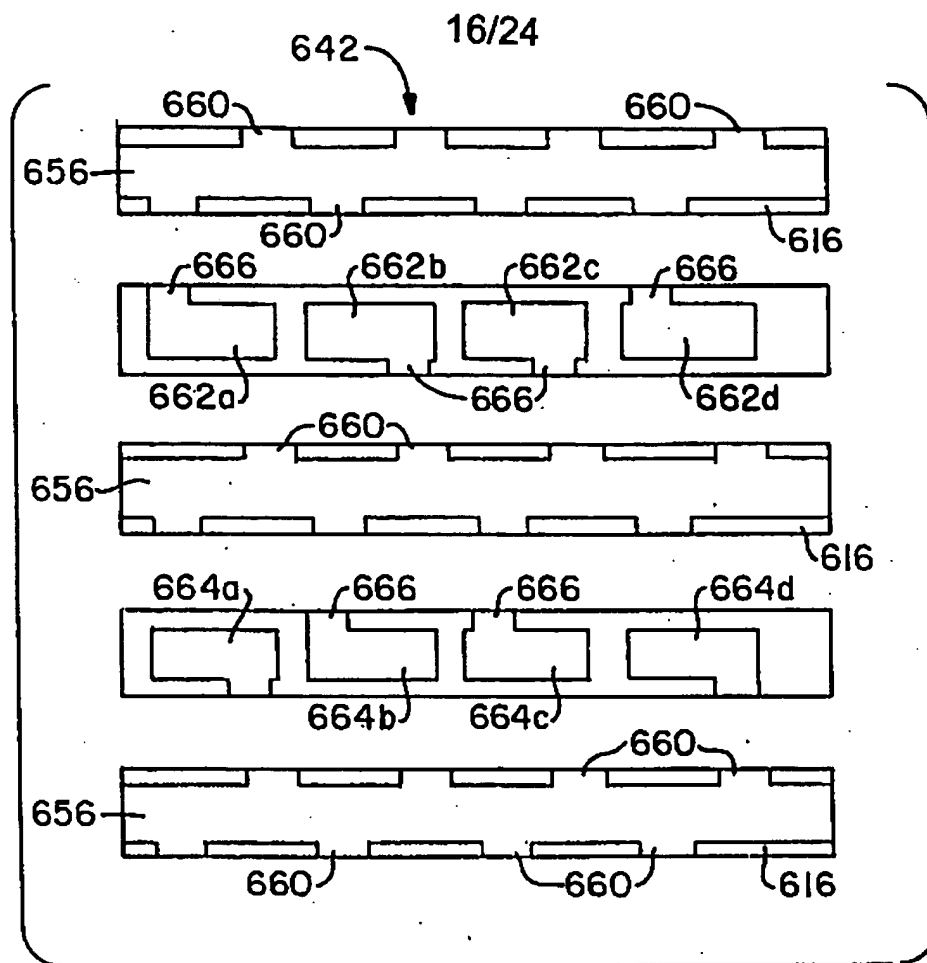


FIG. -29

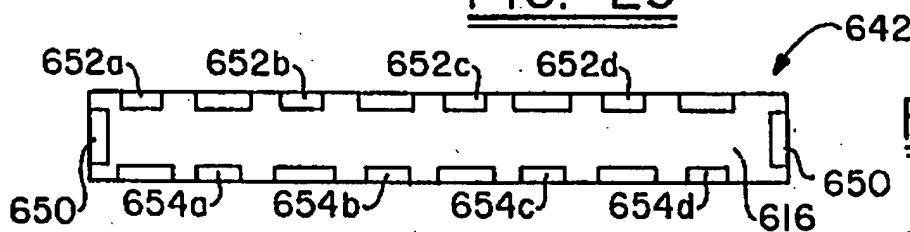


FIG. -30A

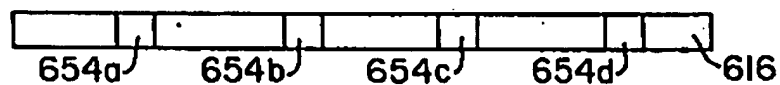


FIG. -30B

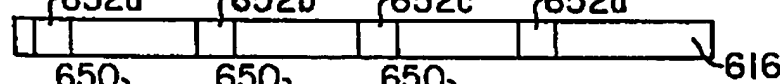


FIG. -30C

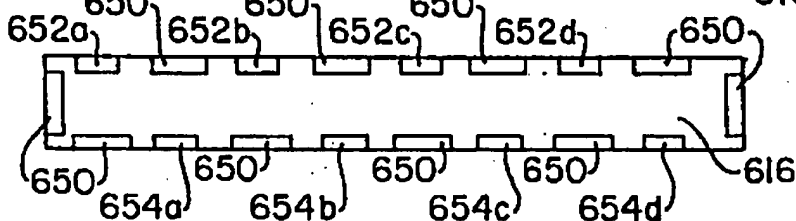
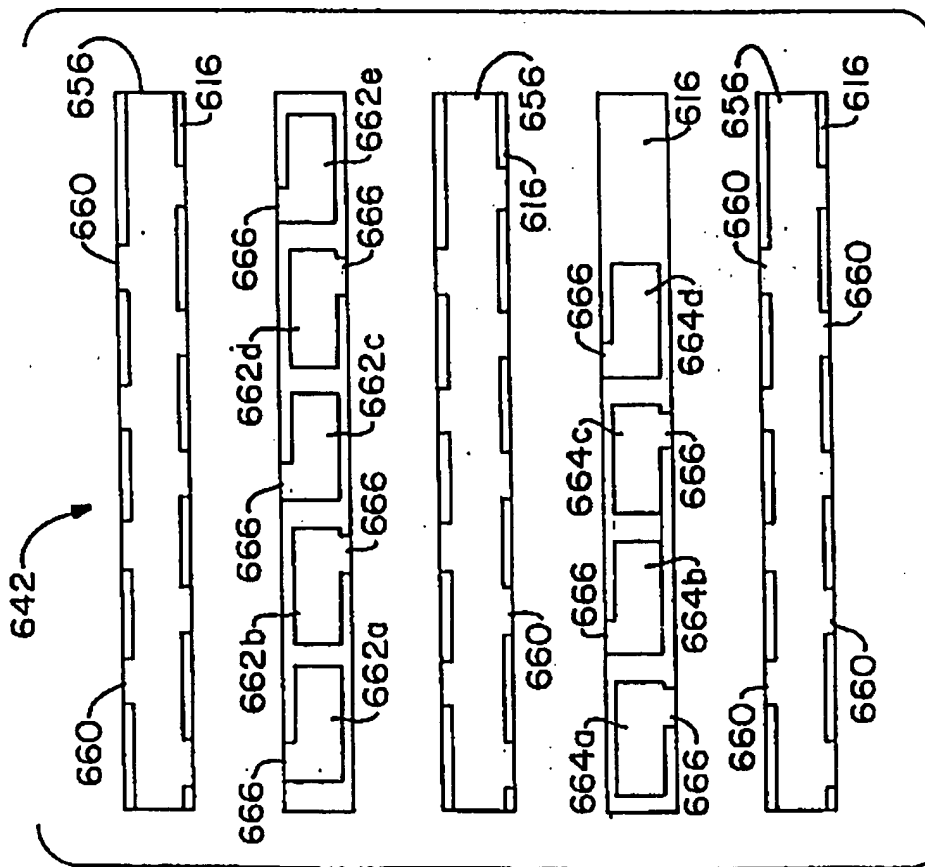
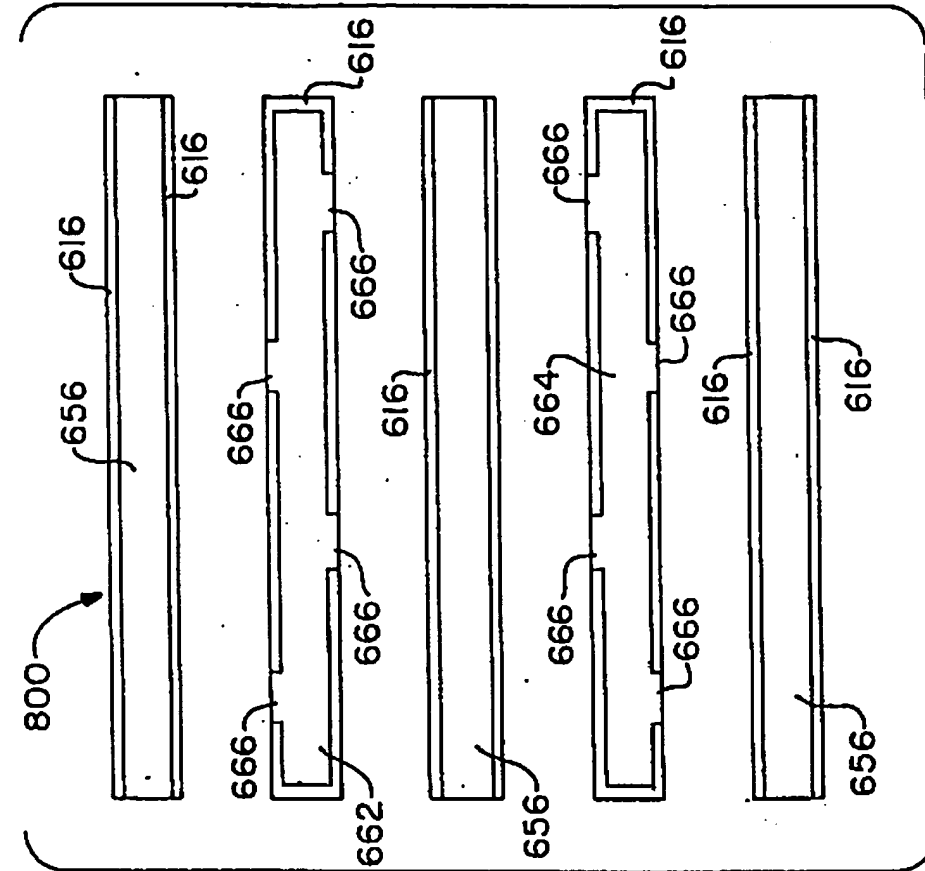


FIG. -30D



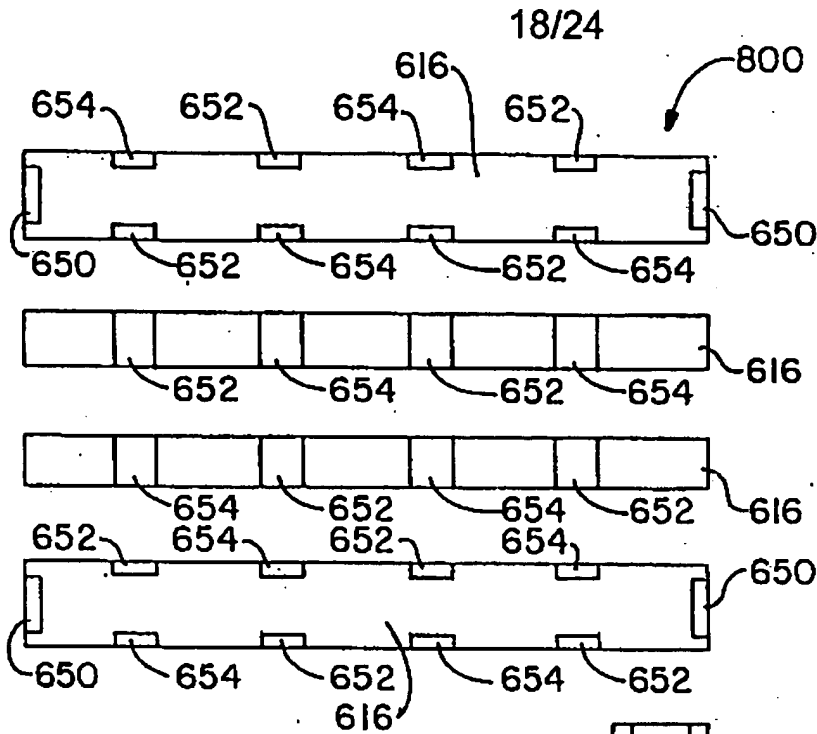


FIG.- 33A

FIG.- 33B

FIG.- 33C

FIG.- 33D

FIG.- 33E

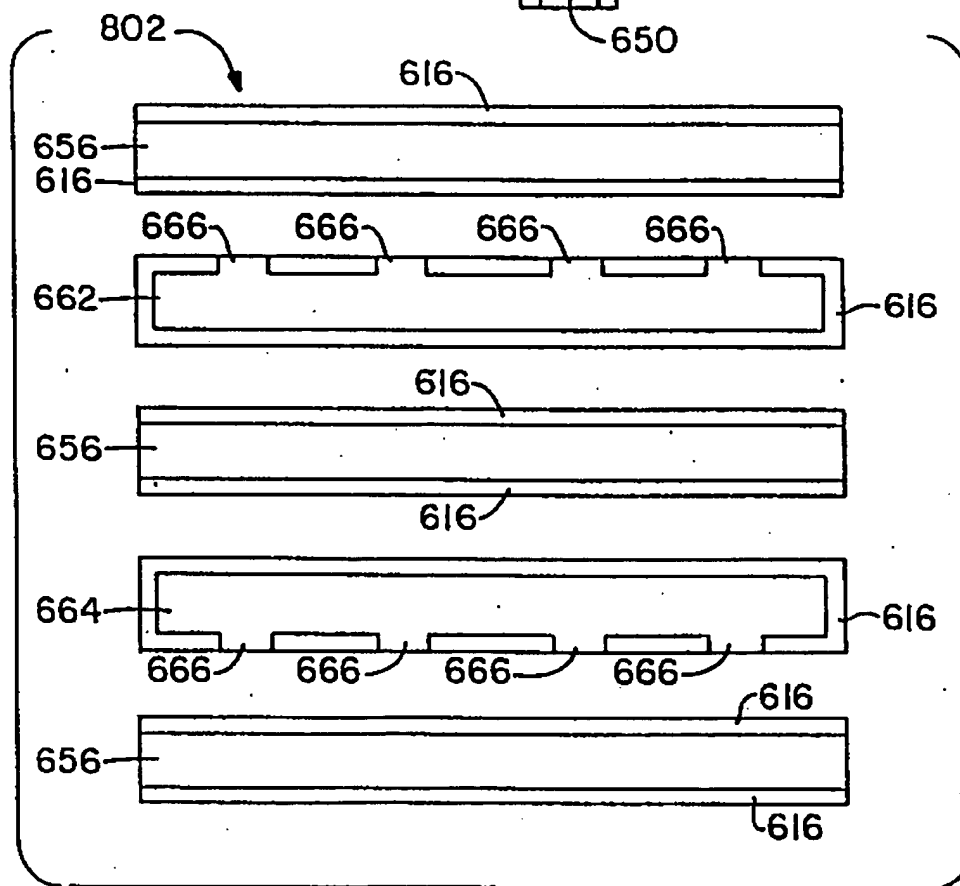


FIG.- 34

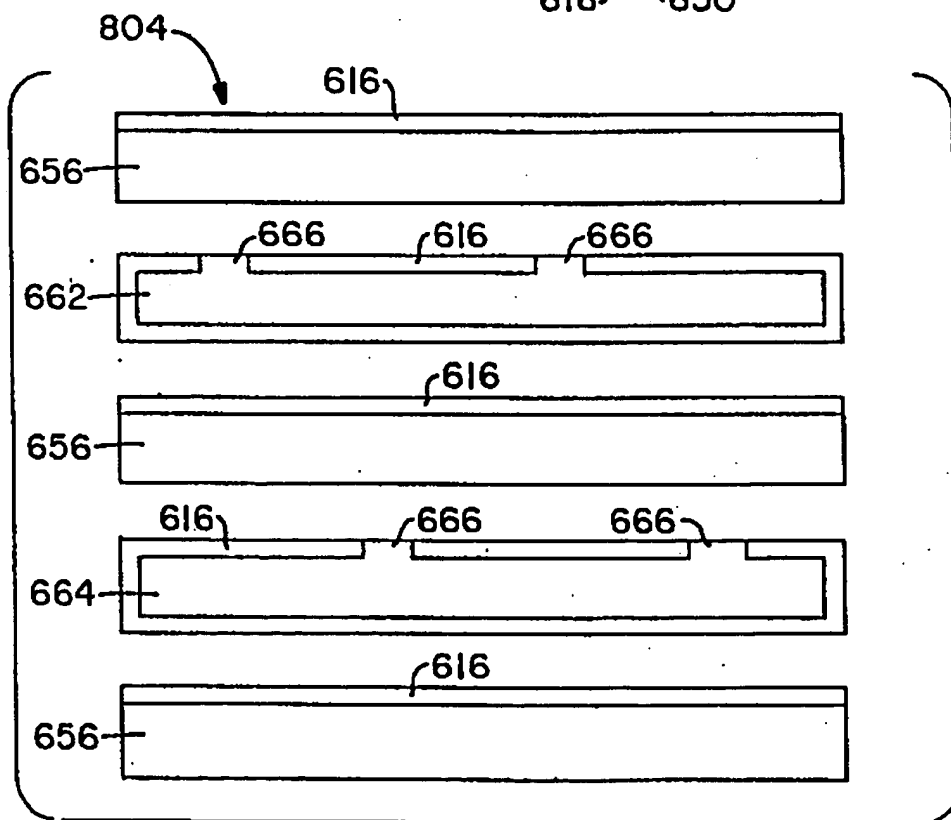
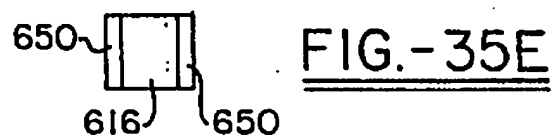
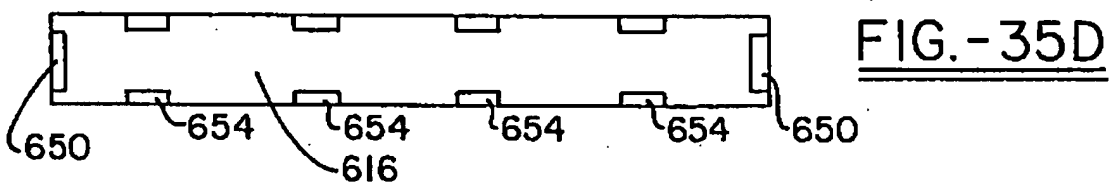
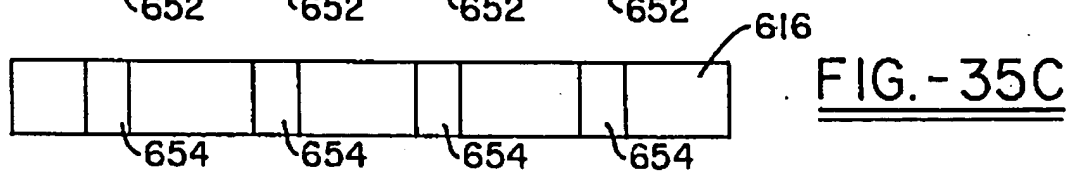
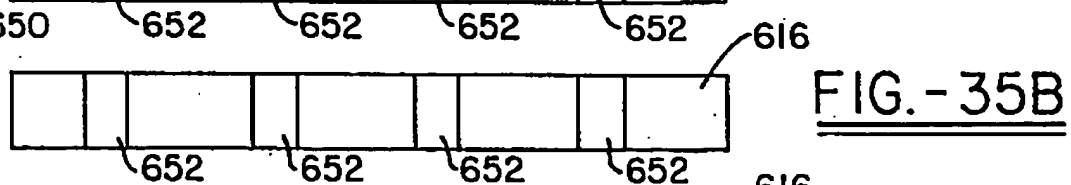
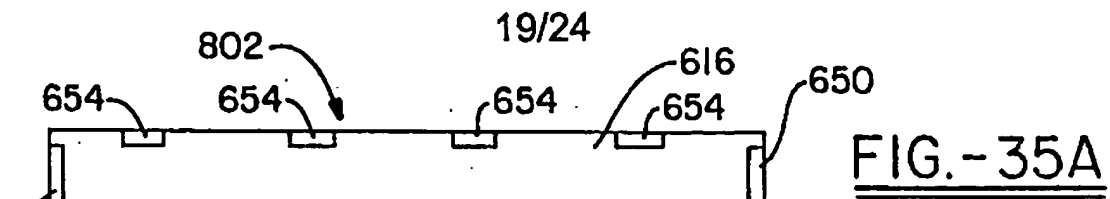


FIG. - 36

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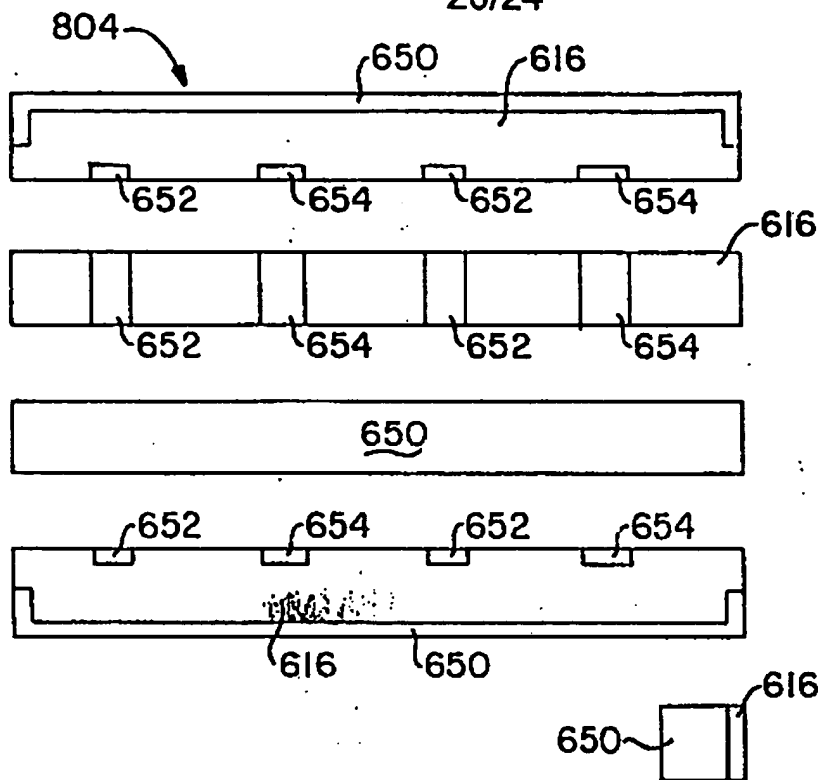


FIG.-37A

FIG.-37B

FIG.-37C

FIG.-37D

FIG.-37E

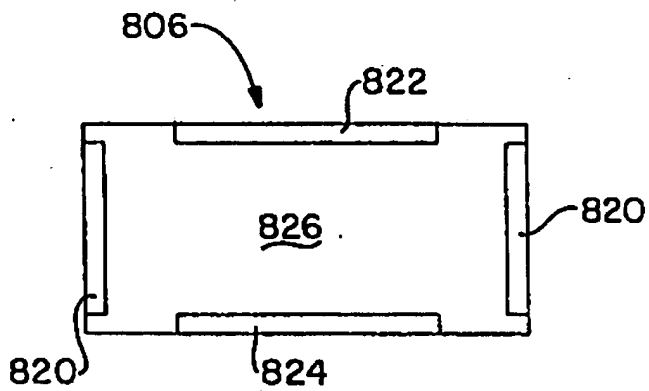


FIG.-40A

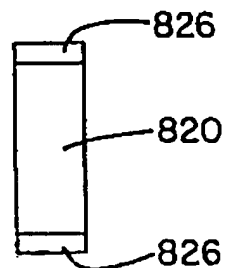


FIG.-40C

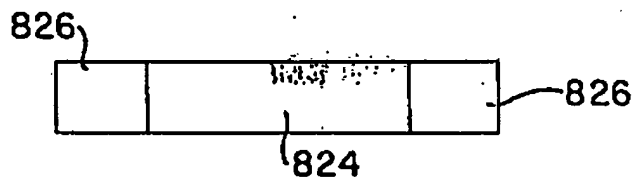


FIG.-40B

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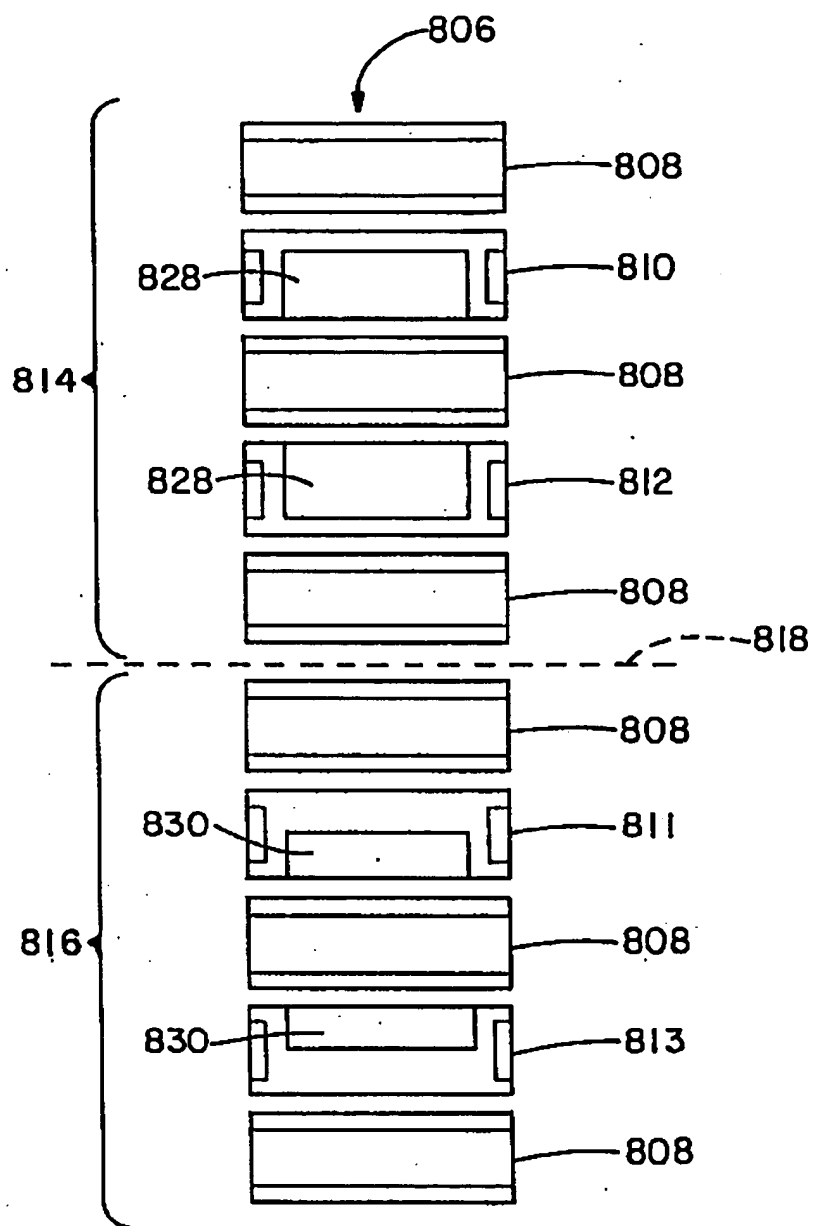


FIG.-38

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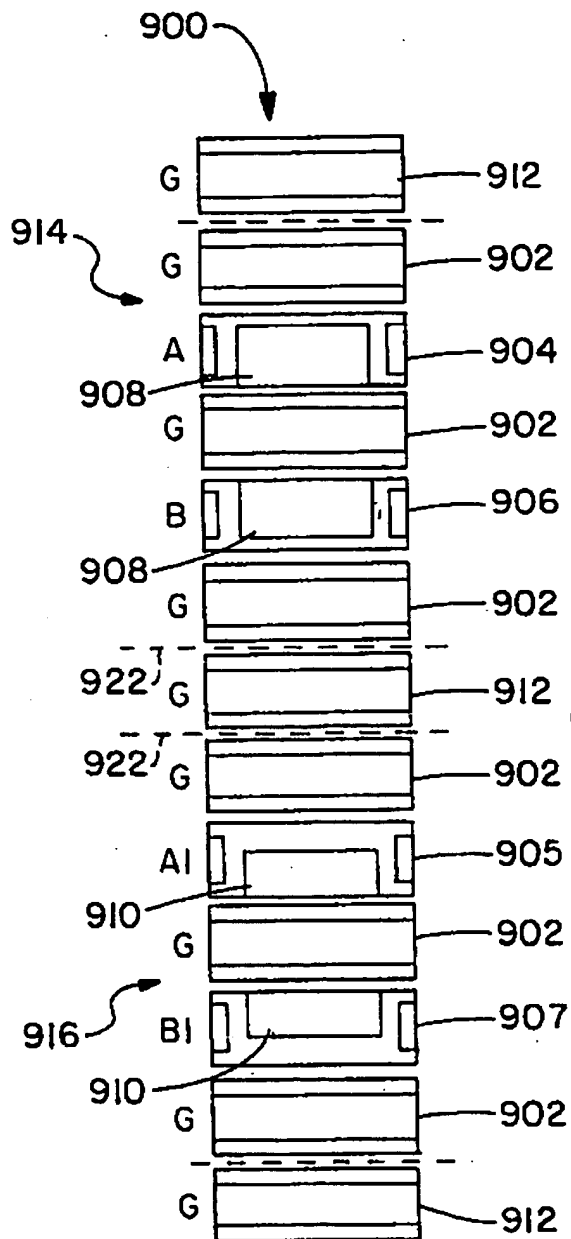


FIG.-41A

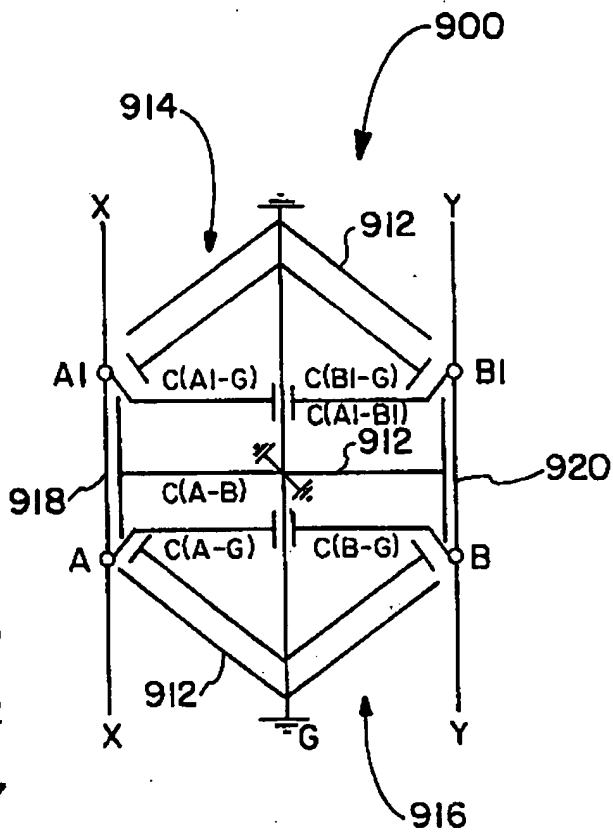
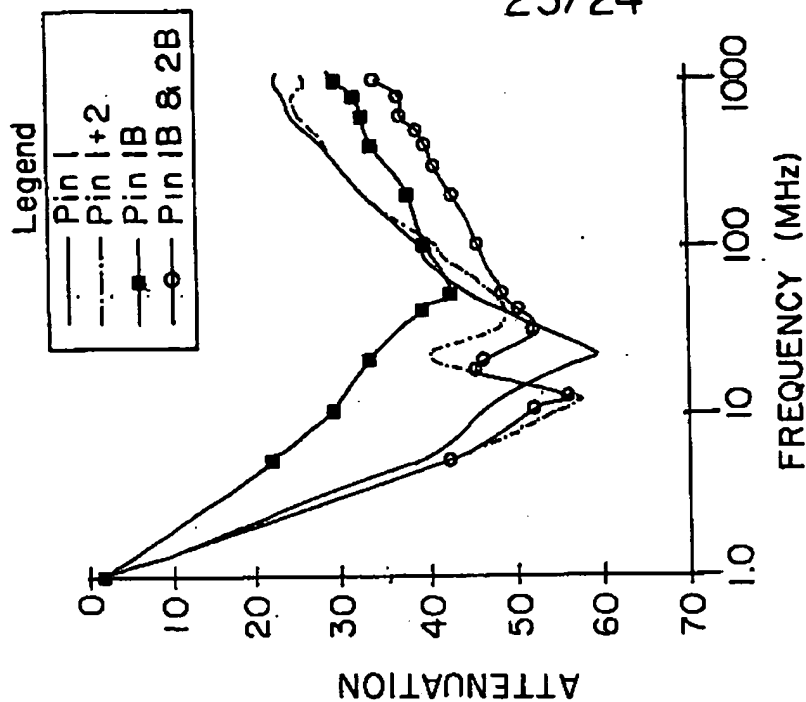


FIG. -41B

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FIG.-4IDFIG.-4IC

MHz	0.1uf			0.1uf-4.8nf		
	Pin 1	Pin 1-2	Pin 1B	Pin 1B	Pin 1B & 2B	
Frequency						
1	2	2	2	2	2	
2						
3						
4						
5	39	42	22	22	42	
6						
7						
8						
9						
10	46	55	29	29	52	
12		57			56	
17					45	
20	57	40	33	33	46	
22	58.8					
30		47			52	
40	47.5	48.5	39	39	50	
50			42	42	48	
60	42	45				
70						
80	39	41.5				
90						
100	38	40	39	39	45	
200	32	32	37	37	42	
300					40	
400	27.5	28	33	33	39	
500					38	
600	24	25	32	32	36	
700						
800	23	24	31	31	36	
900						
1000	22	25.5	29	29	33	
2000	24	22	24	24		

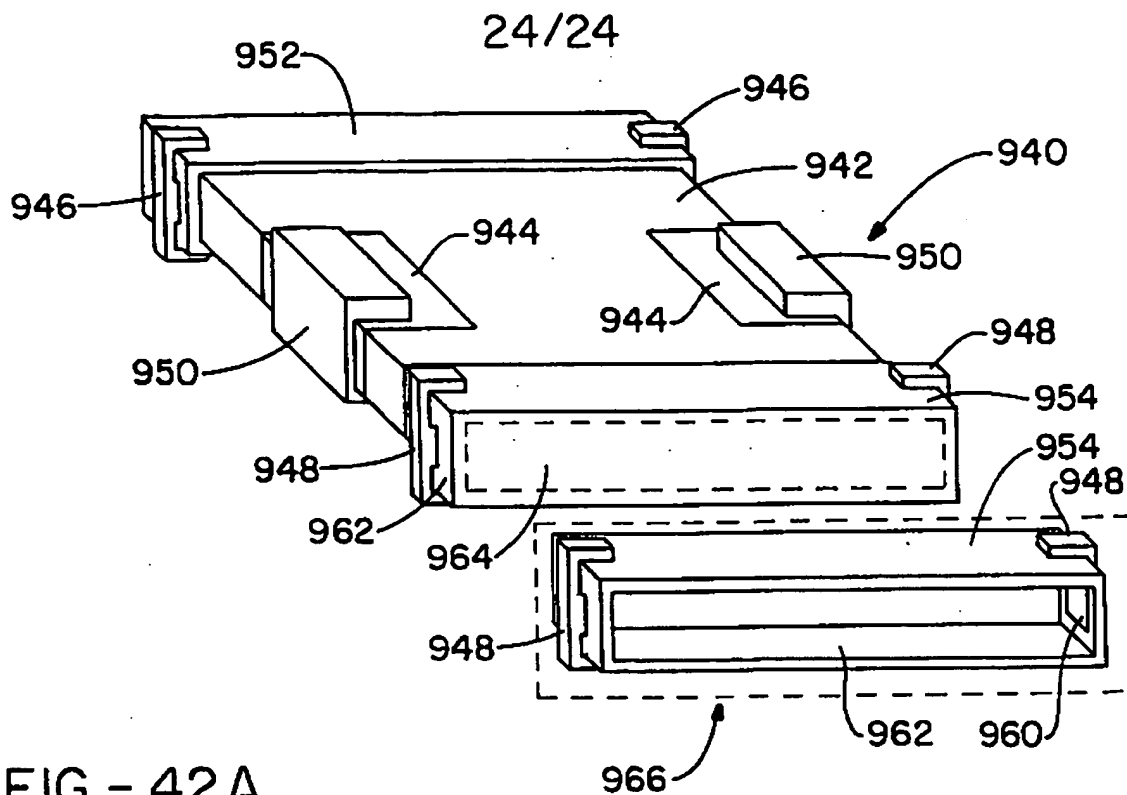
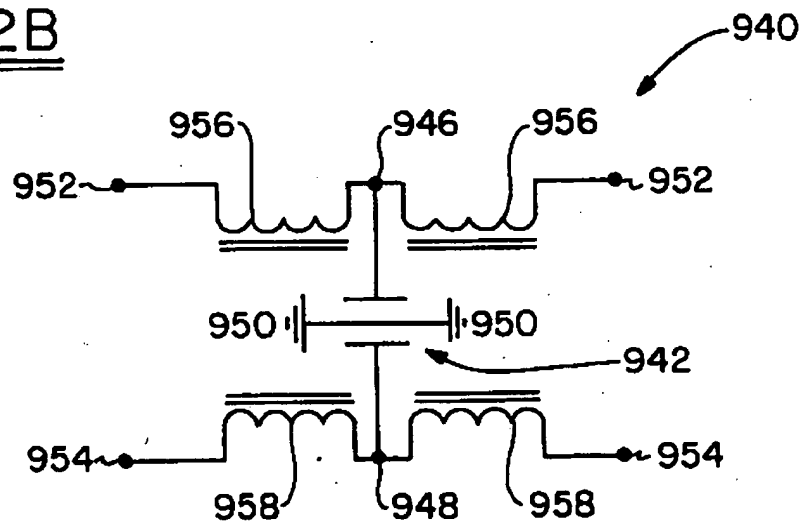
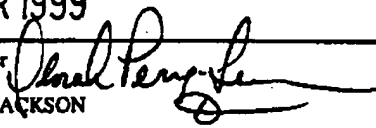


FIG. - 42B



INTERNATIONAL SEARCH REPORT

International application No.
PCT/US99/01040

A. CLASSIFICATION OF SUBJECT MATTER		
IPC(6) : H02H 9/00 US CL : 361/118 According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED		
Minimum documentation searched (classification system followed by classification symbols) U.S. : 361/118,56,78,91,111,113,115,117,119,127		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used) USPTO APS search terms: plates, electrodes, filter, dielectric, protect, circuit		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 3,842,374 A (SCHLICKE) 15 OCTOBER 1974 (15.10.74), see entire document	1-51
A	US 4,262,317 A (BAUMBACH) 14 APRIL 1981 (14.04.81), see entire document	1-51
A	US 4,335,417 (SAKSHAUG et al) 15 JUNE 1982 (15.06.82), see entire document	1-51
<input type="checkbox"/> Further documents are listed in the continuation of Box C. <input type="checkbox"/> See patent family annex.		
* Special categories of cited documents:	*T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention *A* document defining the general state of the art which is not considered to be of particular relevance *E* earlier document published on or after the international filing date *L* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) *O* document referring to an oral disclosure, use, exhibition or other means *P* document published prior to the international filing date but later than the priority date claimed *X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone *Y* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art *Z* document member of the same patent family	
Date of the actual completion of the international search 29 MARCH 1999		Date of mailing of the international search report 19 APR 1999
Name and mailing address of the ISA/US Commissioner of Patents and Trademarks Box PCT Washington, D.C. 20231 Facsimile No. (703) 305-3230		Authorized officer  STEPHEN JACKSON Telephone No. (703) 308-1782



BARKER BRETTCELL

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2001 Jefferson Davis Highway
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VA 22202
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Our ref.

YCJ0112 ✓

Please reply to Birmingham

11 July 2005

Dear Rick,

US Patent Application No. 10/503,788 ✓
Entitled: "Improved Surgical Devices and Methods of Use" ✓
In the name of Gursharan Singh Chana

Please find enclosed, by airmail, certified copies of the priority documents in connection with the above-mentioned US Patent Application as requested.

Yours sincerely

Mrs. Yvonne C. Johnson

TH

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Consultants: S. William Stonehouse Colin D. Kinton Christopher J. Spall Richard N.H. Callaghan John P. Hooper Donald J. Attfield

Document 11

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P01/7700 0.00-0219696.2

1/77

Request for grant of a patent

(See the notes on the back of this form. You can also get
an explanatory leaflet, from the Patent Office to help
you fill in this form)

The Patent Office

Cardiff Road
Newport
Gwent NP9 1RH

1. Your reference	LPT0276		
2. Patent application number (The Patent Office will fill in this part)	0219696.2		
3. Full name, address and postcode of the or of each applicant (<u>underline all surnames</u>)	Gursharan Singh Chana Kenwood 57 Bracebridge Road Sutton Coldfield B74 2SL		
Patents ADP number (if you know it) If the applicant is a corporate body, give the country/state of its incorporation			
4. Title of the invention	Improved Surgical Devices and Methods of Use.		
5. Name of your agent (if you have one)	Barker Brettell		
"Address for service" in the United Kingdom to which all correspondence should be sent (including the postcode)	138 Hagley Road Edgbaston Birmingham B16 9PW		
Patents ADP number (if you know it)	7442494002		
6. If you are declaring priority from one or more earlier patent applications, give the country and the date of filing of the or of each of these earlier applications and (if you know it) the or each application number	Country	Priority application number (if you know it)	Date of Filing (day/month/year)
7. If this application is divided or otherwise derived from an earlier UK application, give the number and the filing date of the earlier application	Number of earlier application		Date of filing (day/month/year)
8. Is a statement of inventorship and of right to grant of a patent required in support of this request (Answer 'Yes' if: a) any applicants named in part 3 is not an inventor, or b) there is an inventor who is not named as an applicant, or c) any named applicant is a corporate body. See note (d))	NO		

08336646001

Patents Form 1/77

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Patent
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- 5 MAR 2002

NEWPORT

1/

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The Patent Office
Cardiff Road
Newport
Gwent NP9 1L

1. Your reference

LPT0197

2. Patent application number

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05 MAR 2002

0205043.3

3. Full name, address and postcode of the or of each applicant (underline all surnames)

Gursharan Singh Chana
Kenwood
57 Bracebridge Road
Sutton Coldfield
B74 2SL

05MAR02 E700713-1 D02806
P01/7700 0.00-0205043..

Patents ADP number (if you know it) 08336646001

If the applicant is a corporate body, give the country/state of its incorporation

4. Title of the invention

IMPROVED SURGICAL DEVICES AND METHODS OF USE

5. Name of your agent (if you have one)

Barker Brettell

"Address for service" in the United Kingdom to which all correspondence should be sent (including the postcode)

138 Hagley Road
Edgbaston
Birmingham
B16 9PW

Patents ADP number (if you know it)

7442494002

6. If you are declaring priority from one or more earlier patent applications, give the country and the date of filing of the or of each of these earlier applications and (if you know it) the or each application number

Country

Priority application number
(if you know it)Date of Filing
(day/month/year)

7. If this application is divided or otherwise derived from an earlier UK application, give the number and the filing date of the earlier application

Number of earlier application

Date of filing
(day/month/year)

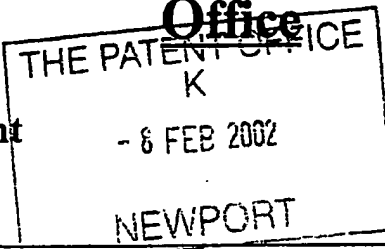
8. Is a statement of inventorship and of right to grant of a patent required in support of this request (Answer 'Yes' if:

No

a) any applicant named in part 3 is not an inventor, or
b) there is an inventor who is not named as an applicant, or
c) any named applicant is a corporate body.
See note (d))

1977

The
Patent
Office



1

Request for grant of a patent

(See the notes on the back of this form. You can also get an explanatory leaflet, from the Patent Office to help you fill in this form)

Th

Cardin
Newport
Gwent NR

1. Your reference

LPT0159

09FEB02 E694382-16 D02806

2. Patent application number
(The Patent Office will fill in this)

0202934.6

0417700 0.00 0202934.6

8 FEB 20

3. Full name, address and postcode of the or of each applicant (underline all surnames)

~~Guru Sharon Chana~~

GURSHARAN SINGH CH

Kenwood

57 Bracebridge Road

Sutton Coldfield

B74 2SL

Patents ADP number (if you know it)

08236646001

If the applicant is a corporate body, give the country/state of its incorporation

832048001

4. Title of the invention

IMPROVED SURGICAL DEVICES AND METHODS OF USE

5. Name of your agent (if you have one)

Barker Brettell

"Address for service" in the United Kingdom to which all correspondence should be sent (including the postcode)

138 Hagley Road

Edgbaston

Birmingham

B16 9PW

Patents ADP number (if you know it)

7442494002

6. If you are declaring priority from one or more earlier patent applications, give the country and the date of filing of the or of each of these earlier applications and (if you know it) the or each application number

Country

Priority application number
(if you know it)

Date of Filing
(day/month/year)

7. If this application is divided or otherwise derived from an earlier UK application, give the number and the filing date of the earlier application

Number of earlier application

Date of filing
(day/month/year)

8. Is a statement of inventorship and of right to grant of a patent required in support of this request (Answer 'Yes' if:

No

a) any applicant named in part 3 is not an inventor, or
b) there is an inventor who is not named as an applicant, or
c) any named applicant is a corporate body.
See note (d))